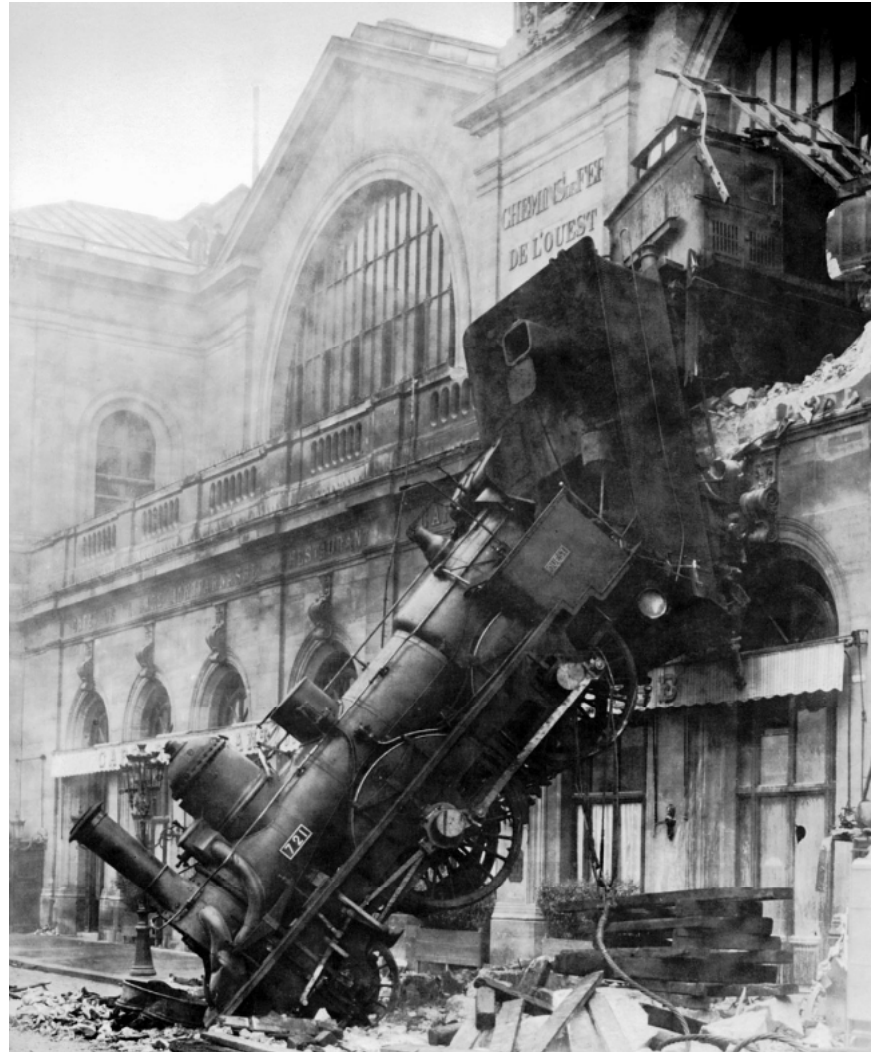


Reliability and risk analysis



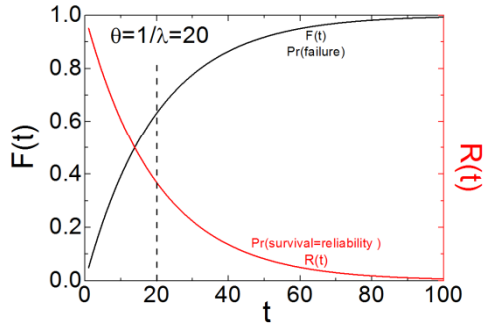
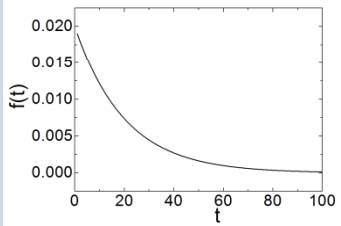
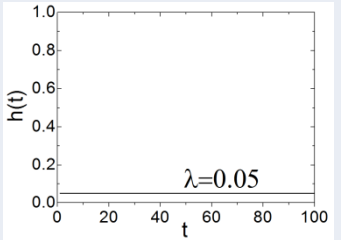
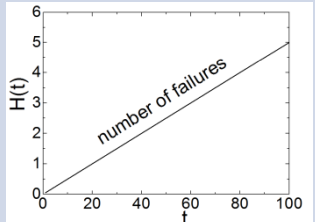
Luis Carlos Pardo . C2.4

Summary

0.- Remeber

- 1.- Bayes theorem
- 2.- Maximum likelihood method
- 3.- Estimation of reliability parameters from tests
- 4.- Confidence limits of parameters
- 5.- Accelerated life testing
- 6.- Determination of distribution models
- 7.- Empirical determination of survivor function
- 8.- Reliability growth
- 9.- Strength-stress models

Summary of important quantities

| | Description | example | graph |
|-------------------------------|----------------------------------------------------------|-----------------------------------|---------------------------------------------------------------------------------------|
| cdf $R_T(t)$ | Reliability function or Survival function | $R_T(t) = e^{-\lambda t}$ |  |
| cdf $F_T(t)$ | Failure probability Lifetime distribution function | $F_T(t) = 1 - e^{-\lambda t}$ | |
| pdf $f_T(t)$ | Probability to fail Between t and t+dt | $f_T(t) = \lambda e^{-\lambda t}$ |  |
| Pdf $\lambda(t)$ $h(t)$ | Failure rate or Hazard function | $h(t) = \lambda$ |  |
| cdf $H(t)$ | Number of failures | $H(t) = \lambda \cdot t$ |  |

Summary of important relations

$$R_T(t) = 1 - F_T(t)$$

$$f_T(t) = \frac{dF_T(t)}{dt}$$

$$f_T(t)$$

$$F_T(t) = \int_0^t f_T(t) dt$$

failure probability

$$h(t) = \frac{f_T(t)}{R(t)}$$

$$H(t)$$

$$h(t) = \frac{dH(t)}{dt}$$

failure ratio

$$h(t)$$

$$H(t) = \int_0^t h(t) dt$$

Summary of important relations

$$F_T(t) = 1 - e^{-\lambda t}$$

Failure probability

$$f_T(t) = \frac{dF_T(t)}{dt}$$

$$f_T(t)$$

Failure probability at t

$$F_T(t) = \int_0^t f_T(t) dt$$

$$h(t) = \frac{f_T(t)}{R(t)}$$

Number of failures

$$H(t) = \lambda \cdot t = \# \text{ failures}$$

$$h(t) = \frac{dH(t)}{dt}$$

failure ratio

$$h(t) = \lambda = \frac{\text{failures}}{\text{time}}$$

$$H(t) = \int_0^t h(t) dt$$

Summary

- 1.- Bayes theorem**
- 2.- Maximum likelihood method**
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And finally: Bayes theorem

From the “multiplication” of probability:

$$\text{prob}(A, B) = \text{prob}(A) \cdot \text{prob}(B | A)$$

$$\text{prob}(A, B) = \text{prob}(B) \cdot \text{prob}(A | B)$$

dividing the two equations we get:



Bayes theorem

$$\text{prob}(A | B) = \frac{\text{prob}(B | A) \text{prob}(A)}{\text{prob}(B)}$$

That help us to reverse probabilities...

Bayes theorem

$$\text{prob}(H | D) = \frac{\text{prob}(D | H) \text{prob}(H)}{\text{prob}(D)}$$

Posterior prob(H|D):

What you want to know is the probability that your hypothesis is true given the data

Likelihood (or L) prob(D|H):

What you know is your hypothesis. And therefore you can calculate the probability that your data “gathers” around your hypothesis

Prior prob(H):

You might want to include any prior information about your hypothesis

Evidence (E) prob(D):

Is “simply” a normalization factor... we will come back when doing model selection

The ubiquitous χ^2

Bayes theorem



Likelihood
Probability that our data
describes the hypothesis

Prior
Our forehand knowledge

$$P(H | D) = \frac{P(D | H) \cdot P(H)}{P(D)}$$

T. Bayes.

Posterior
Probability that the hypothesis is true
given the experimental data

Evidence
Normalization factor

In our case is very simple...

Bayes theorem



Likelihood
Probability that our data
describes the hypothesis

Maximum ignorance Prior

$$P(H | D) \propto \frac{P(D | H) \cdot P(H)}{P(D)}$$

T. Bayes.

Posterior
Probability that the hypothesis is true
given the experimental data

We only care about proportionality

Thus, assuming a maximum ignorance prior:

$$\mathit{prob}(H \mid D) \propto \mathit{prob}(D \mid H) = L$$

But what is exactly H, in practice?

It is a function and the parameters inside it

$$H_i(a, b) = a + bx_i$$

Summary

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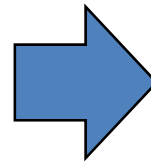
Parameter estimation

We would like to estimate the best estimate of a quantity, given some data.

Let's define the posterior as:

$$\text{prob}(X | \{data\}) = P$$

The best estimate of X is given by a maximum in its probability and thus



$$\left. \frac{dP}{dX} \right|_{X_0} = 0$$

We want now to expand P as a Taylor series, since P varies too fast we take the logarithm of P

$$L = \ln(P) = \ln(\text{prob}(X | \{data\}))$$

The Taylor expansion of L is:

$$L = L(X_0) + \frac{1}{2} \left. \frac{d^2 L}{dX^2} \right|_{X_0} (X - X_0)^2 + \dots$$

Taking the first term we get for P:

$$\text{prob}(X | \{data\}) \approx A \exp \left[\frac{1}{2} \left. \frac{d^2 L}{dX^2} \right|_{X_0} (X - X_0)^2 \right]$$

Let's compare with a gaussian

$$\text{prob}(X | \{data\}) \approx A \exp \left[\frac{(X - X_0)^2}{2\sigma^2} \right]$$

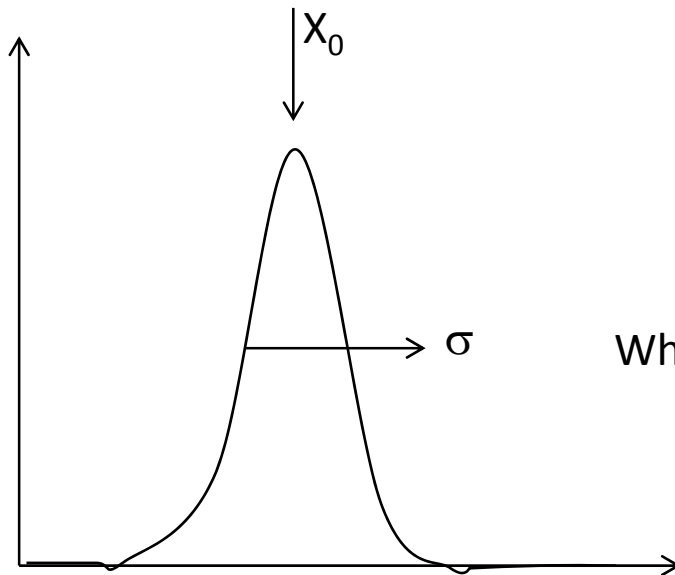
Taking the first term we get for P:

Comparing

$$\text{prob}(X | \{data\}) \approx A \exp \left[\frac{1}{2} \frac{d^2 L}{dX^2} \Big|_{X_0} (X - X_0)^2 \right]$$

Let's compare with a gaussian

$$\text{prob}(X | \{data\}) \approx A \exp \left[-\frac{(X - X_0)^2}{2\sigma^2} \right]$$



$$X = X_0 \pm \sigma$$

$$\sigma = \left(-\frac{d^2 L}{dX^2} \Big|_{X_0} \right)^{-1/2}$$

Where $\frac{d^2 L}{dX^2} \Big|_{X_0}$ is always negative, so: no problem ;-)

Value plus error comes from a Taylor series

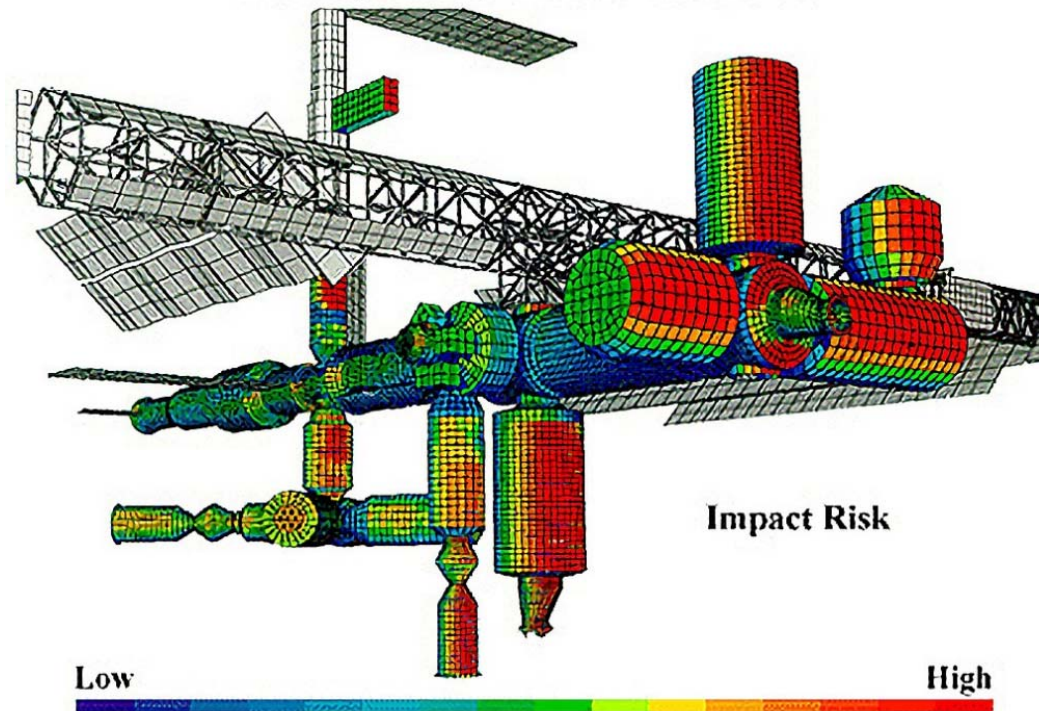
Summary

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**Let's perform tests to quantify risk analysis...
before sending the ISS to the space!!!!**

International Space Station

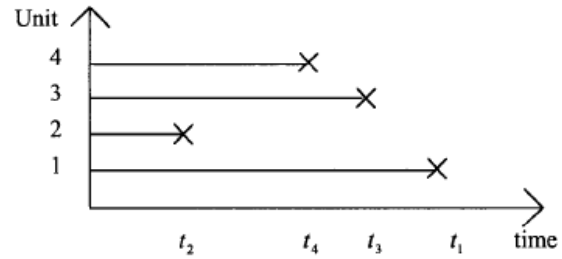
Probability of No Impacts From a > 1 cm \varnothing Debris



Types of tests:

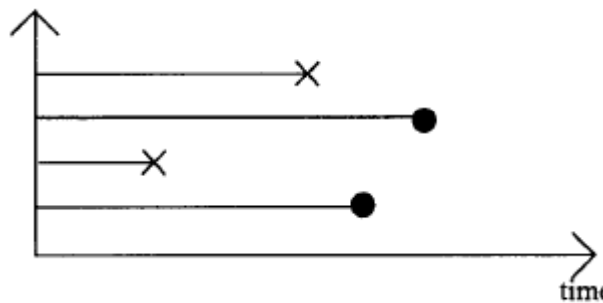
Let's assume that we perform a test on $n=4$ components

Complete data sets

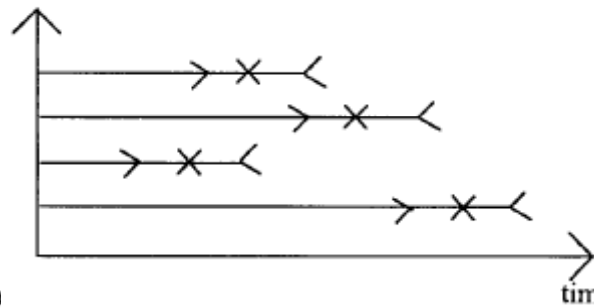


Censored data sets

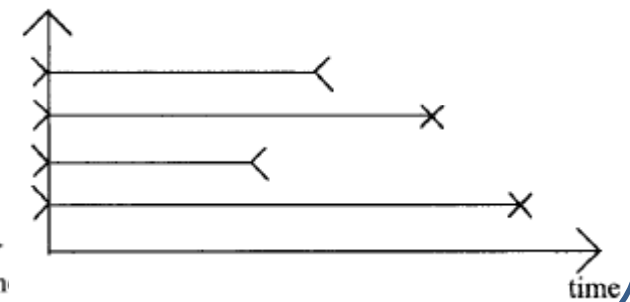
Right censored



Interval censored



Leftcensored

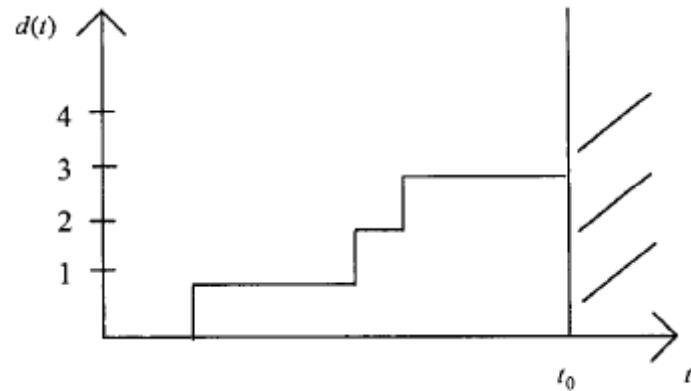


Types of tests:

Test plans

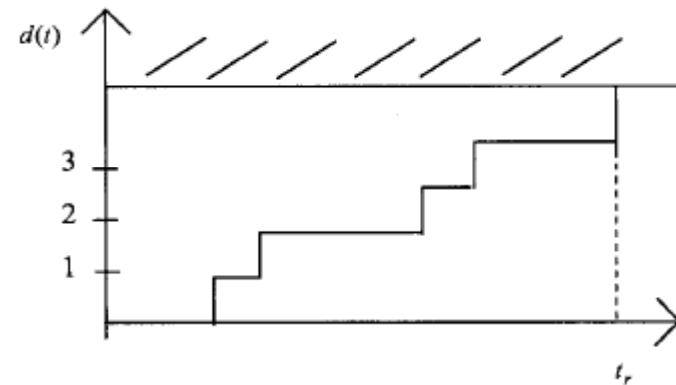
Type I

Testing up to a given time t_0

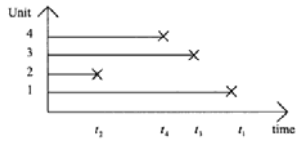


Type II

Testing up to a given r -th failure



They can also be with (R) or without (W) replacement



Determine the failure ratio λ , or its inverse, the **Mean Time To Failure** MTTF τ for n equal units in the case of **non-censored** data

We calculate the **likelihood** that

$$L = \prod_{i=1}^n \lambda e^{-\lambda t_i} = \lambda e^{-\lambda t_1} \cdot \lambda e^{-\lambda t_2} \cdot \lambda e^{-\lambda t_3} \dots \lambda e^{-\lambda t_n} = \lambda^n e^{-\lambda T} \leftarrow \boxed{T = \sum_{i=1}^n t_i}$$

we take the **logarithm**

$$\ln L = \ln \left(\lambda^n e^{-\lambda T} \right) = n \ln \lambda - \lambda T$$

we make the **derivative**

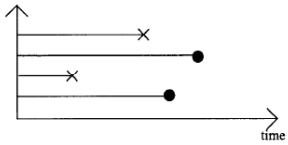
$$\frac{\partial \ln L}{\partial \lambda} = \ln \left(\lambda^n e^{-\lambda T} \right) = \frac{\partial (n \ln \lambda - \lambda T)}{\partial \lambda} = \frac{n}{\lambda} - T$$

we **set it to zero** (find the maximum)

$$\frac{n}{\hat{\lambda}} - T = 0$$

we finally find the **most probable value** for λ

$$\hat{\lambda} = \frac{n}{T}$$



Determine the failure ratio λ , or its inverse, the **Mean Time To Failure** MTTF τ for n equal units in the case of **right-censored** data type I (until t_0)

We calculate the **likelihood** that

$$L = \prod_{i=1}^r \underbrace{f(t_i | \lambda)}_{\text{failure}} \prod_{i=r+1}^n \underbrace{R(t_0 | \lambda)}_{\text{time right-censored}} = \lambda^r e^{-\lambda \sum_{i=1}^r t_i} e^{-\lambda(n-r)t_0} = \lambda^r e^{-\lambda T} \quad \leftarrow \quad T = \sum_{i=1}^r t_i + (n-r)t_0$$

we take the **logarithm**

$$\ln L = \ln(\lambda^r e^{-\lambda T}) = r \ln \lambda - \lambda T$$

we make the **derivative**

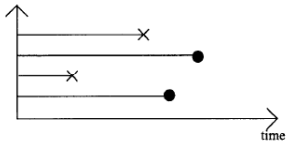
$$\frac{\partial \ln L}{\partial \lambda} = \ln(\lambda^r e^{-\lambda T}) = \frac{\partial (r \ln \lambda - \lambda T)}{\partial \lambda} = \frac{r}{\lambda} - T$$

we **set it to zero** (find the maximum)

$$\frac{r}{\hat{\lambda}} - T = 0$$

we finally find the **most probable value** for λ

$$\hat{\lambda} = \frac{r}{T}$$



Determine the failure ratio λ , or its inverse, the **Mean Time To Failure** MTTF τ for n equal units in the case of **right-censored** data type II (until r units fail)

We calculate the **likelihood** that

$$L = \prod_{i=1}^r \underbrace{f(t_i | \lambda)}_{\text{failure}} \prod_{i=r+1}^n \underbrace{R(t_i | \lambda)}_{\text{right-censored}} = \lambda^r e^{-\lambda \sum_{i=1}^r t_i} e^{-\lambda \sum_{i=r+1}^n t_i} = \lambda^r e^{-\lambda T} \quad \leftarrow \quad T = \sum_{i=1}^n t_i + (n-r)t_r$$

we take the **logarithm**

$$\ln L = \ln(\lambda^r e^{-\lambda T}) = r \ln \lambda - \lambda T$$

we make the **derivative**

$$\frac{\partial \ln L}{\partial \lambda} = \ln(\lambda^r e^{-\lambda T}) = \frac{\partial (r \ln \lambda - \lambda T)}{\partial \lambda} = \frac{r}{\lambda} - T$$

we **set it to zero** (find the maximum)

$$\frac{r}{\hat{\lambda}} - T = 0$$

we finally find the **most probable value** for λ

$$\hat{\lambda} = \frac{r}{T}$$

...BUT YOU DO NOT WANT TO STOP PRODUCTION until r components fail

Determine the failure ratio λ , or its inverse, the **Mean Time To Failure** MTTF τ for n equal units in the case of **right-censored** data type I (until t_0)
WITH REPLACEMENT

Let's do it for a single component $n=1$ that is replaced each time it fails

$n=1$

$$L = \lambda e^{-\lambda t_1} \lambda e^{-\lambda(t_2-t_1)} \lambda e^{-\lambda(t_3-t_2)} \dots \lambda e^{-\lambda(t_0-t_r)} = \lambda^r e^{-\lambda t_0}$$



... for n components

$$L = \lambda^r e^{-\lambda n t_0} = \lambda^r e^{-\lambda T} \quad \leftarrow \boxed{T = n t_0}$$

$n>1$

doing the same calculations as before...

we finally find the **most probable value** for λ

$$\hat{\lambda} = \frac{r}{T}$$

...BUT YOU DO NOT WANT TO STOP PRODUCTION until r components fail

Determine the failure ratio λ , or its inverse, the **Mean Time To Failure** MTTF τ for n equal units in the case of **right-censored** data type II (until r -th failure)
WITH REPLACEMENT

Let's do it for a single component $n=1$ that is replaced each time it fails

$n=1$

$$L = \lambda e^{-\lambda t_1} \lambda e^{-\lambda(t_2-t_1)} \lambda e^{-\lambda(t_3-t_2)} \dots \lambda e^{-\lambda(t_0-t_r)} = \lambda^r e^{-\lambda t_0}$$



... for n components

$$L = \lambda^r e^{-\lambda n t_0} = \lambda^r e^{-\lambda T} \quad \leftarrow \boxed{T = n t_r}$$

$n>1$

doing the same calculations as before...

we finally find the **most probable value** for λ

$$\hat{\lambda} = \frac{r}{T}$$

summarizing: We want to keep the notation $\hat{\lambda} = \frac{r}{T}$

so, we change the meaning of T...

not censored, no replacement $T = \sum_{i=1}^n t_i$

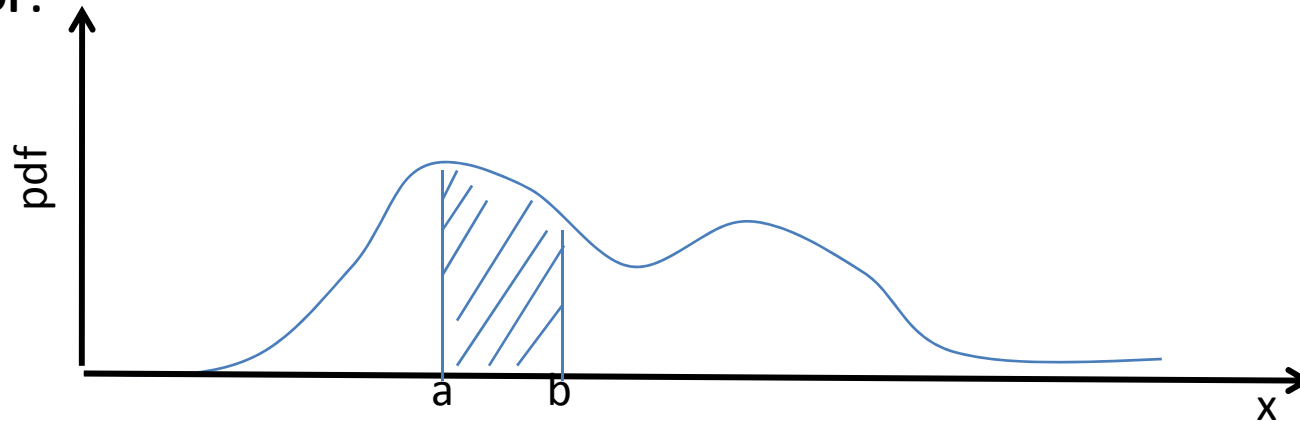
| | Censored Type I (unit t_0) | Censored Type II (unit r -th failure) |
|---------------------|-------------------------------------|-----------------------------------------|
| Without replacement | $T = \sum_{i=1}^n t_i + (n - r)t_0$ | $T = \sum_{i=1}^n t_i + (n - r)t_r$ |
| With replacement | $T = nt_0$ | $T = nt_r$ |

Summary

- 1.- Bayes theorem
- 2.- Maximum likelihood method
- 3.- Estimation of reliability parameters from tests
- 4.- Confidence limits of parameters:
normal distribution

Confidence intervals: the general case

Let's consider a PDF:



Relation with probabilities

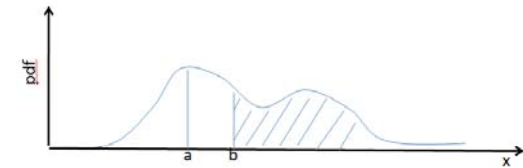
$$p(a < x < b) = \int_a^b f(x) dx$$

Therefore

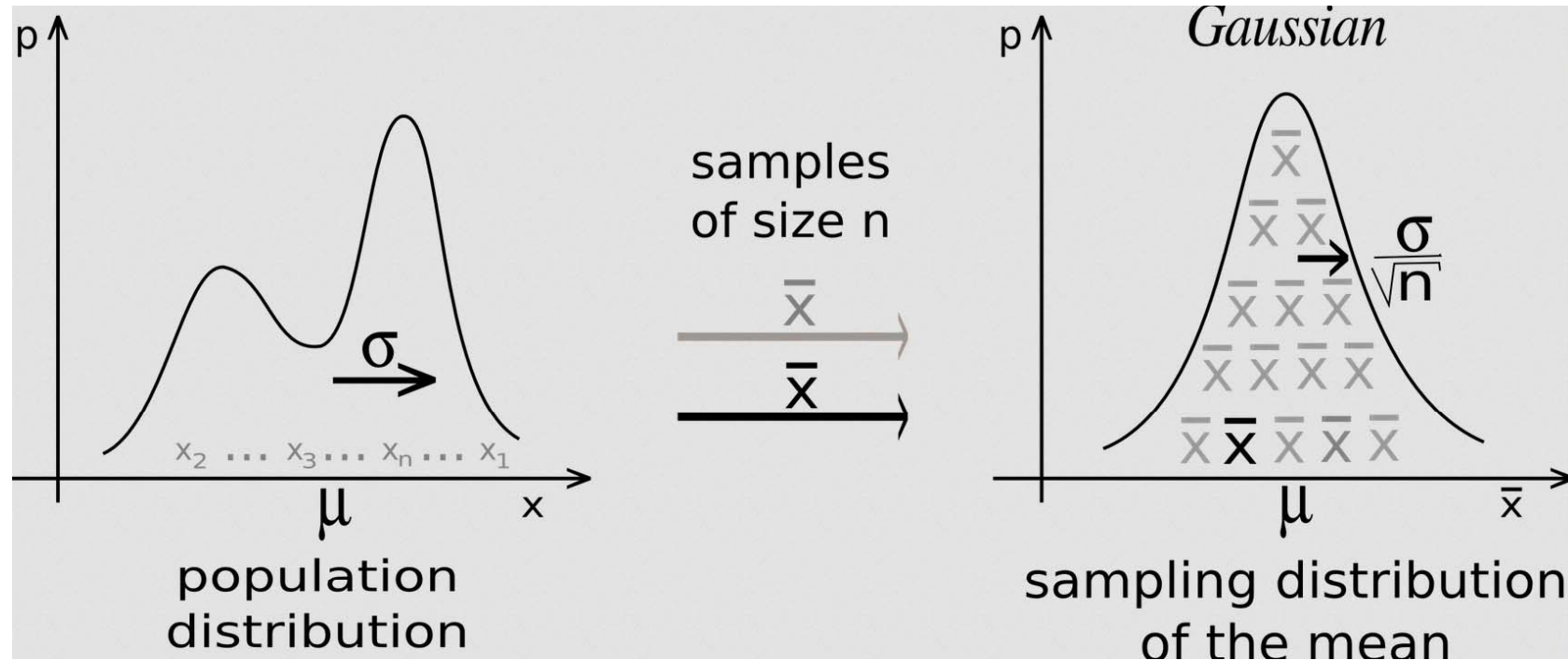
$$\int_{-\infty}^{\infty} f(x) dx = 1$$

P-value for b (one side)

$$p(x > b) = \int_b^{\infty} f(x) dx$$



Central limit theorem

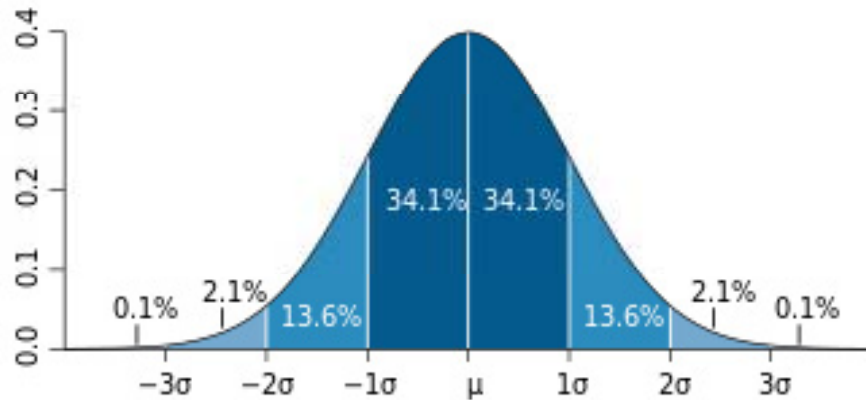


The distribution of the mean tends to be gaussian when increasing n
no matters the pdf that originated the mean!!!!

This is the good and the bad thing from statistics is based on the normal PDF!!!!

Standard Normal distribution

Standard Normal distribution ($\mu=0, \sigma=1$)



$$f(x) = \frac{1}{\sqrt{2\pi}} \exp\left(-\frac{1}{2}x^2\right)$$

Therefore, defining a “z-value”
for the whole population as $z = \frac{x - \mu}{\sigma_x}$

Therefore, defining a
“z-value” for n units

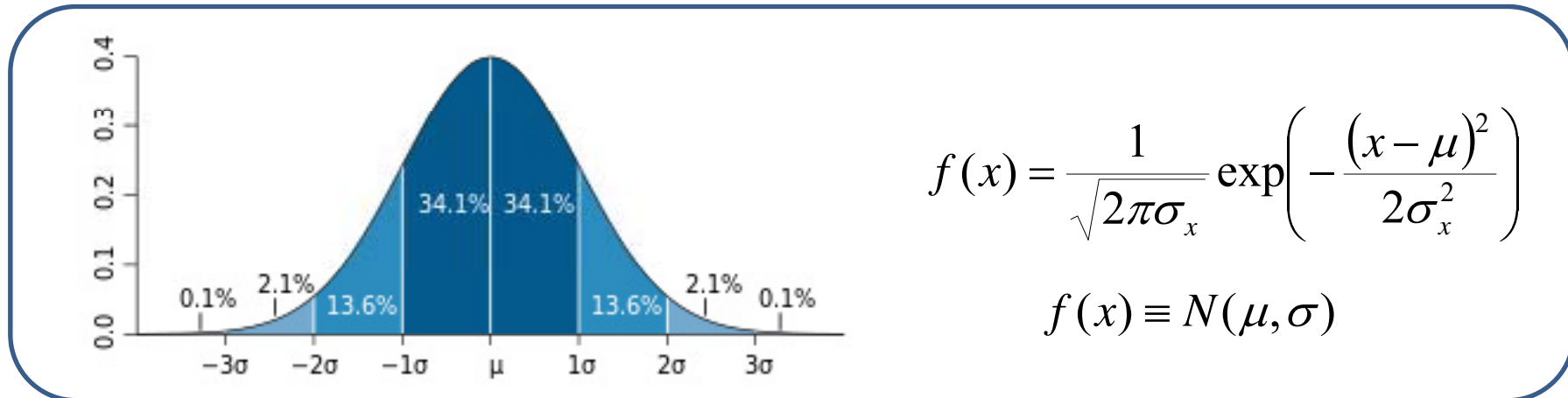
$$z = \frac{\bar{X} - \mu}{\frac{\sigma_x}{\sqrt{n}}}$$

$$f(x) = \frac{1}{\sqrt{2\pi\sigma_x}} \exp\left(-\frac{1}{2}\left(\frac{x - \mu}{\sigma_x}\right)^2\right) \Rightarrow f(z) = \frac{1}{\sqrt{2\pi}} \exp\left(-\frac{1}{2}z^2\right)$$

Z follows a **standard** normal distribution function...

Confidence intervals: the normal case

Normal distribution



Relation with probabilities

$$p(-\sigma_x < x < \sigma_x) = \int_{-\sigma}^{\sigma} f(x)dx = 68.2\%$$

P-value for normal distribution for a value a: is related with the variance

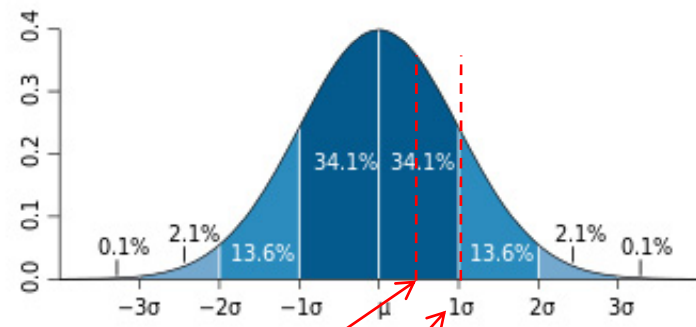
$$p(-\sigma_x < x < \sigma_x) = \int_{-\sigma}^{\sigma} f(x)dx = 68.2\%$$

So we have a relationship between confidence intervals and probability!

There is a 68,2% of chances that your real value is inside your “error “

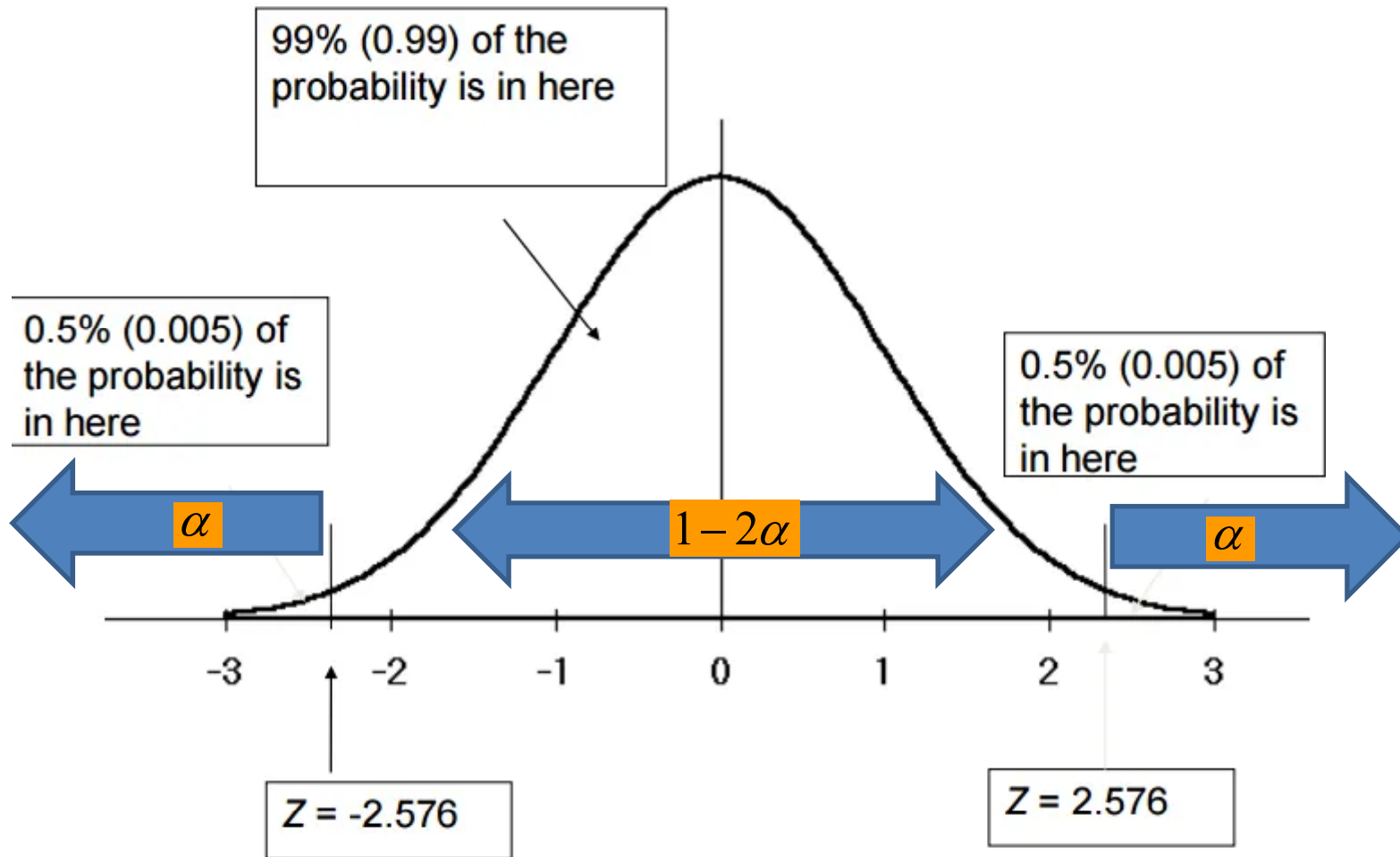
(assuming that x has a normal distribution;-)

standard normal table



| z | +0.00 | +0.01 | +0.02 | +0.03 | +0.04 | +0.05 | +0.06 | +0.07 | +0.08 | +0.09 |
|-----|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 0.0 | 0.00000 | 0.00399 | 0.00798 | 0.01197 | 0.01595 | 0.01994 | 0.02392 | 0.02790 | 0.03188 | 0.03586 |
| 0.1 | 0.03983 | 0.04380 | 0.04776 | 0.05172 | 0.05567 | 0.05962 | 0.06356 | 0.06749 | 0.07142 | 0.07535 |
| 0.2 | 0.07926 | 0.08317 | 0.08706 | 0.09095 | 0.09483 | 0.09871 | 0.10257 | 0.10642 | 0.11026 | 0.11409 |
| 0.3 | 0.11791 | 0.12172 | 0.12552 | 0.12930 | 0.13307 | 0.13683 | 0.14058 | 0.14431 | 0.14803 | 0.15173 |
| 0.4 | 0.15542 | 0.15910 | 0.16276 | 0.16640 | 0.17003 | 0.17364 | 0.17724 | 0.18082 | 0.18439 | 0.18793 |
| 0.5 | 0.19146 | 0.19497 | 0.19847 | 0.20194 | 0.20540 | 0.20884 | 0.21226 | 0.21566 | 0.21904 | 0.22240 |
| 0.6 | 0.22575 | 0.22907 | 0.23237 | 0.23565 | 0.23891 | 0.24215 | 0.24537 | 0.24857 | 0.25175 | 0.25490 |
| 0.7 | 0.25804 | 0.26115 | 0.26424 | 0.26730 | 0.27035 | 0.27337 | 0.27637 | 0.27935 | 0.28230 | 0.28524 |
| 0.8 | 0.28814 | 0.29103 | 0.29389 | 0.29673 | 0.29955 | 0.30234 | 0.30511 | 0.30785 | 0.31057 | 0.31327 |
| 0.9 | 0.31594 | 0.31859 | 0.32121 | 0.32381 | 0.32639 | 0.32894 | 0.33147 | 0.33398 | 0.33646 | 0.33891 |
| 1.0 | 0.34134 | 0.34375 | 0.34614 | 0.34849 | 0.35083 | 0.35314 | 0.35543 | 0.35769 | 0.35993 | 0.36214 |
| 1.1 | 0.36433 | 0.36650 | 0.36864 | 0.37076 | 0.37286 | 0.37493 | 0.37698 | 0.37900 | 0.38100 | 0.38298 |

Confidence interval: $1-2\alpha$



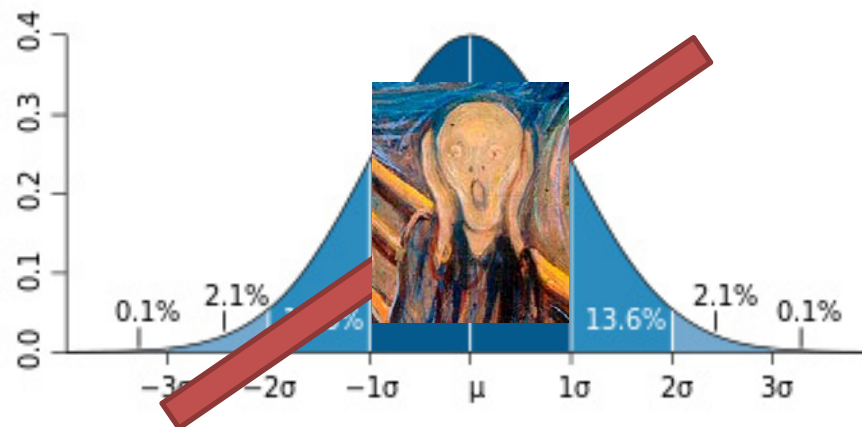
Summary

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Chi-square distribution

Problem

failure ratio does not follows a normal distribution!!!

$$\hat{\lambda} = \frac{r}{T}$$



Solution

... but $2\lambda T$ does follow a given distribution. Let me proudly introduce you the chi-square distribution

Chi-Squared distribution

Do you remember the normal distribution:

$$f(x) = \frac{1}{\sqrt{2\pi\sigma_x}} \exp\left(-\frac{1}{2}\left(\frac{x-\mu}{\sigma_x}\right)^2\right) \Rightarrow f(z) = \frac{1}{\sqrt{2\pi}} \exp\left(-\frac{1}{2}z^2\right)$$

We minimize Z^2 in order to find μ ... the following question arises:

What is the PDF for Z^2 itself?

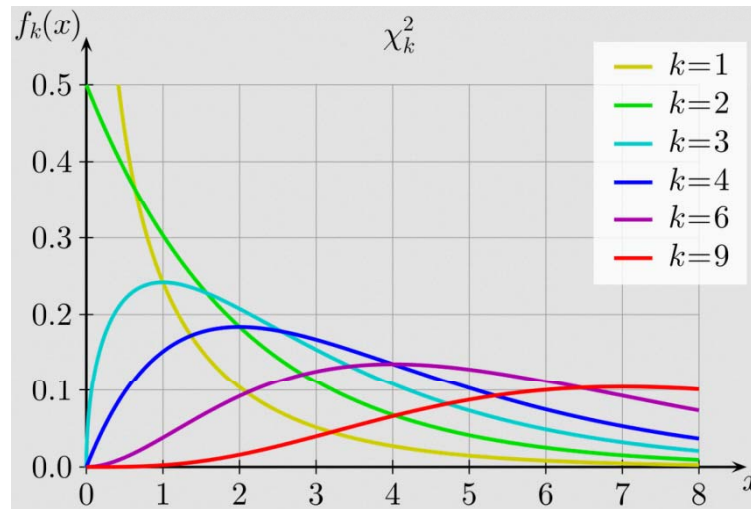
Chi-Squared distribution

If X_i follow a standard normal distribution then $\chi^2 = \underbrace{X_1^2 + X_2^2 + X_3^2 + \dots + X_k^2}$

follow a so called χ^2 distribution with **k degrees of freedom** defined as:

$$f(x) = A \cdot x^{k/2-1} e^{-x/2}$$

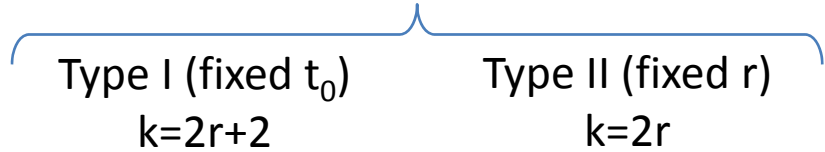
$$A = \frac{1}{2^{k/2} \Gamma(k/2)}$$



$$\mu = k; \text{var} = 2k; \text{max} = k - 2$$

If $k \rightarrow \infty$ then $\frac{\chi^2 - k}{\sqrt{2k}}$ follows a standard normal distribution, i.e. χ^2 follows $N(k, \sqrt{2k})$

$2\lambda T$ is χ^2 distributed with k degrees of freedom



Let's now calculate the confidence limits:

ONE SIDED (lower limit)

Type I (fixed t_0)
 $k=2r+2$

$$P\left[2\lambda T \leq \chi_\alpha^2(2+2r)\right] = \alpha$$

$$P\left[\lambda \leq \frac{\chi_\alpha^2(2+2r)}{2T}\right] = \alpha$$

$\theta = \frac{1}{\lambda}$

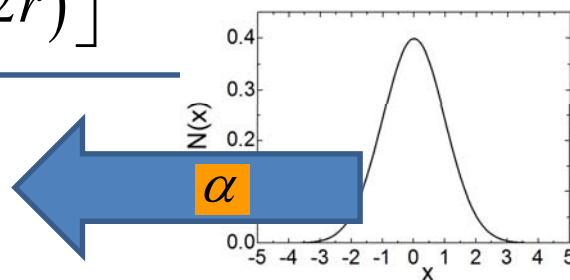
$$P\left[\theta \leq \frac{2T}{\chi_\alpha^2(2+2r)}\right] = \alpha$$

Type I (fixed r)
 $k=2r$

$$P\left[2\lambda T \leq \chi_\alpha^2(2r)\right] = \alpha$$

$$P\left[\lambda \leq \frac{\chi_\alpha^2(2r)}{2T}\right] = \alpha$$

$\theta = \frac{1}{\lambda}$

$$P\left[\theta \leq \frac{2T}{\chi_\alpha^2(2r)}\right] = \alpha$$


$2\lambda T$ is χ^2 distributed with **k** degrees of freedom

Type I (fixed t_0)
 $k=2r+2$

Type II (fixed r)
 $k=2r$

Let's now calculate the confidence limits:

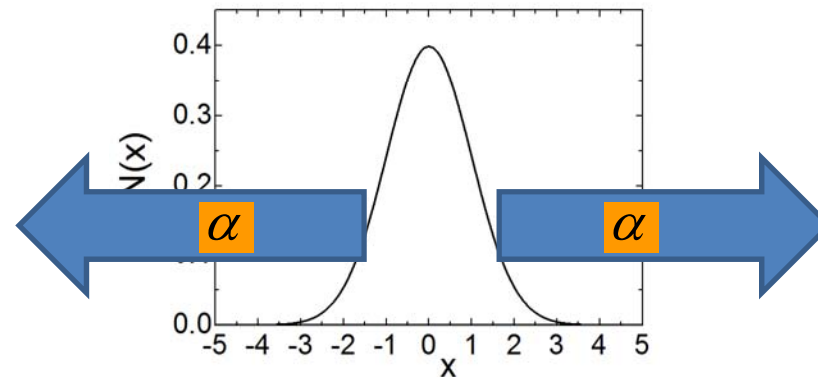
TWO SIDED (lower and upper limit)

Type I (fixed t_0)
 $k=2r+2$

$$P\left[\frac{2T}{\chi_{\frac{\alpha}{2}}^2(2+2r)}\theta \leq \frac{2T}{\chi_{1-\frac{\alpha}{2}}^2(2+2r)}\right] = \alpha$$

Type I (fixed r)
 $k=2r$

$$P\left[\frac{2T}{\chi_{\frac{\alpha}{2}}^2(2r)}\theta \leq \frac{2T}{\chi_{1-\frac{\alpha}{2}}^2(2r)}\right] = \alpha$$



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- 9.- Strength-stress models

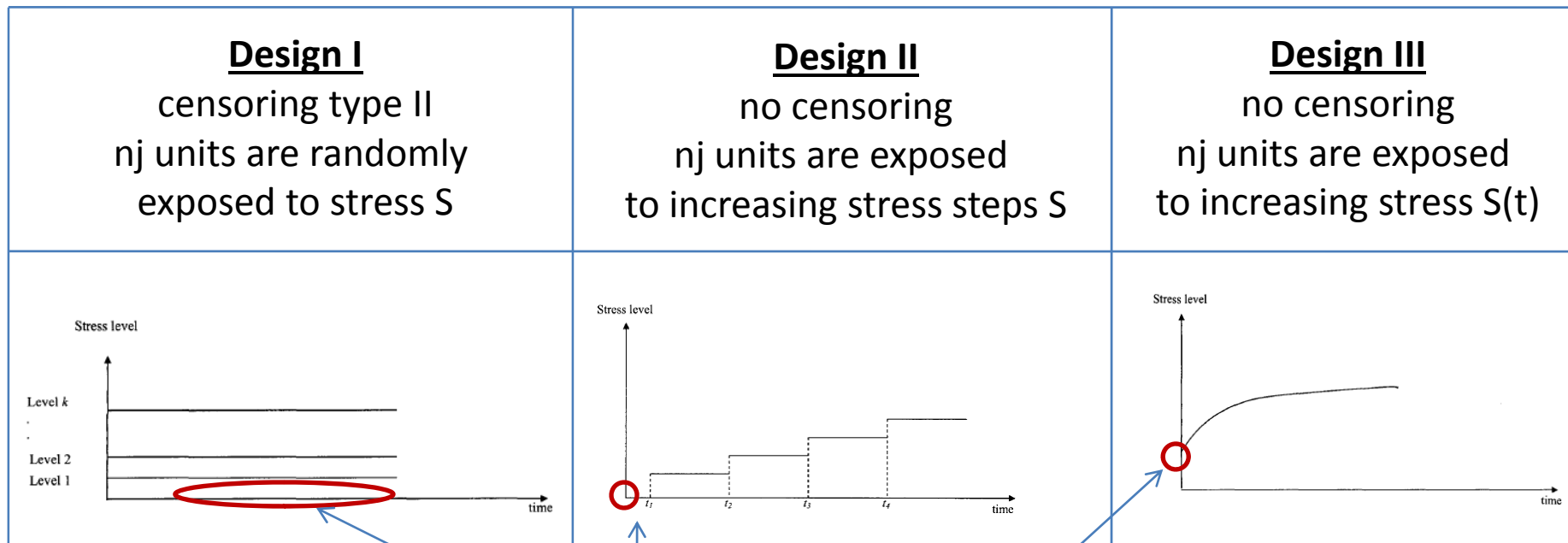
Accelerated Life Tests (ALTs)

Fortunately enough: we cannot wait until the “units” fail...

... so we stress them with voltage, pressure, load, vibration → **stressors S_1, S_2, S_3, \dots**

And each stressor has different levels of actuation, being $S_j^{(0)}$ normal stress

in a general case $S_j^{(0)} < S_j^{(1)} < S_j^{(2)} < S_j^{(3)} \dots S_j^{(k)}$ for stressor $j=1,2,\dots, m$ and levels until k



The idea is to extrapolate to $S_j^{(0)}$

Accelerated Life Tests (ALTs)

Parametric models

Let's quantify our stress accelerated life tests...

Now our functions are affected by stress, therefore:

| | |
|--------------------------------------|-------------------------------------------|
| Lifetime distribution function (CDF) | $F(t; s) = P(T \leq t; s)$ |
| Associated PDF | $f(t; s) = P(t \leq T \leq t + dt; s)$ |
| Survival function | $R(t; s) = 1 - F(t; s)$ |
| Failure rate | $\lambda(t; s) = \frac{f(t; s)}{R(t; s)}$ |

Accelerated Life Tests (ALTs)

Parametric models

Exponential distribution under design I:

Functional proposals for the relation between stress and failure ratio:

$$\lambda(s) = \frac{1}{c} s^a$$

Power rule

- Dielectric breakdown of capacitors
- Fatigue testing

$$\lambda(s) = ce^{-b/s}$$

Arrhenius model

- Thermal aging
- Semiconductor materials

$$\lambda(s) = c \cdot s^{-b/s}$$

Eyring model

- constant thermal stress
-

Accelerated Life Tests (ALTs)

Parametric models for Design I

Design I

censoring type II, n_j units are randomly exposed to stress S

Let's calculate the values of a , c and λ

$S^{(j)}$: is the stress level

n_j : number of units tested at stress level j

r_j : number of units failed under stress j

$T_{j1}, T_{j2}, \dots, T_{jn_j}$ = lifetimes of the n_j tested units

The total time in test is $T_j = \sum_{i=1}^{r_j} T_{ji} + (n_j - r_j)T_{jr_j}$

$$f(T_j) = \frac{dZ_j}{dT_j} A \cdot T_j^{k/2-1} e^{-T_j/2} = 2\lambda$$

As we have seen, Z follows a chi-square distribution with $2r_j$ degrees of freedom

$$Z_j = 2\lambda \left(S^{(j)} \right) T_j$$

$$f(Z_j) = A \cdot Z_j^{k/2-1} e^{-Z_j/2}$$

We change variables from Z to T

$$f(Z) = \frac{dZ}{dT} f(T) = 2\lambda f(T)$$

$$f(T_j) = A \cdot \lambda \left(S^{(j)} \right)^{r_j} T_j^{r_j-1} e^{-\lambda S^{(j)} T_j}$$

The likelihood thus read as:

$$L = f(T_1, \dots, T_k) = \prod_{j=1}^k A \cdot \lambda \left(S^{(j)} \right)^{r_j} T_j^{r_j-1} e^{-\lambda S^{(j)} T_j}$$

Assuming an exponential relationship

$$\lambda \left(S^{(j)} \right) = \frac{1}{c} \left(\frac{S^{(j)}}{S} \right)$$

$$S = \left[\sqrt{\prod_{j=1}^k S^{(j)}} \right]^{r_j / \sum_{i=1}^k r_j}$$

We can now calculate the likelihood, the logarithm and minimize... obtaining

expected value for a

expected value for c

expected value for λ

$$\sum_{j=1}^k \left[\frac{S^{(j)}}{S} \right]^{\hat{a}} \ln \left[\frac{S^{(j)}}{S} \right] = 0$$

$$c = \frac{1}{\sum_{j=1}^k r_j} \sum_{j=1}^k \left[\frac{S^{(j)}}{S} \right]^{\hat{a}} \cdot t_j = 0$$

$$\lambda = \frac{1}{c} \sum_{j=1}^k \left[\frac{S^{(j)}}{S} \right]^{\hat{a}}$$

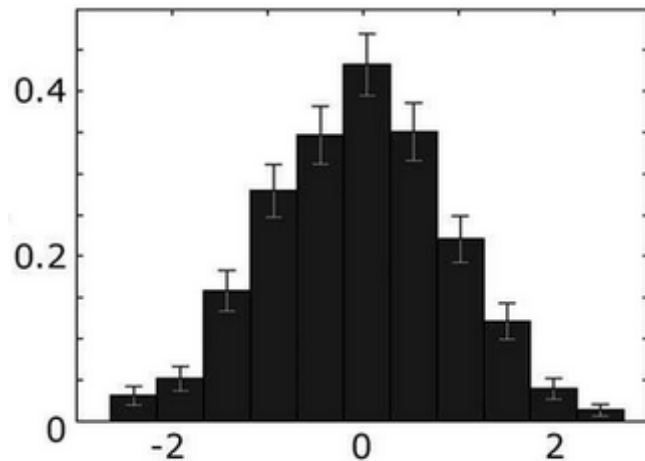
Summary

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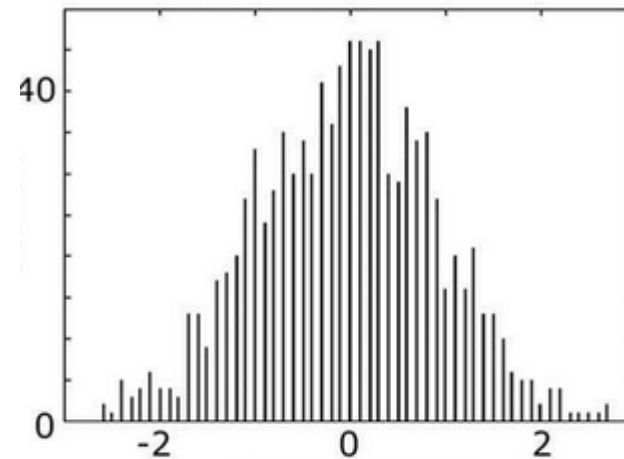
So, we have up to now ASSUMED the distribution $f(t)$, but...
what if the distribution is not known???

Let's assume that there are n units each failing at a time t_i

First we have to distribute them inside boxes: binning
we must therefore decide the size of the binning!



- big bin size
- small error
- few points



- small bin size
- big error
- a lot of points

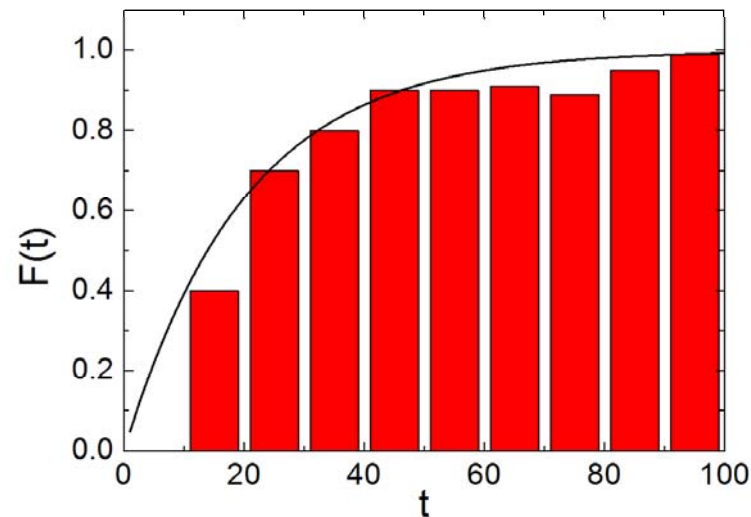
So, we have up to now ASSUMED the distribution $f(t)$, but...
what if the distribution is not known???

Let's assume that there are n units each failing at a time t_i

Now we must see if the obtained curve is a gaussian, or exponential, or weibull...

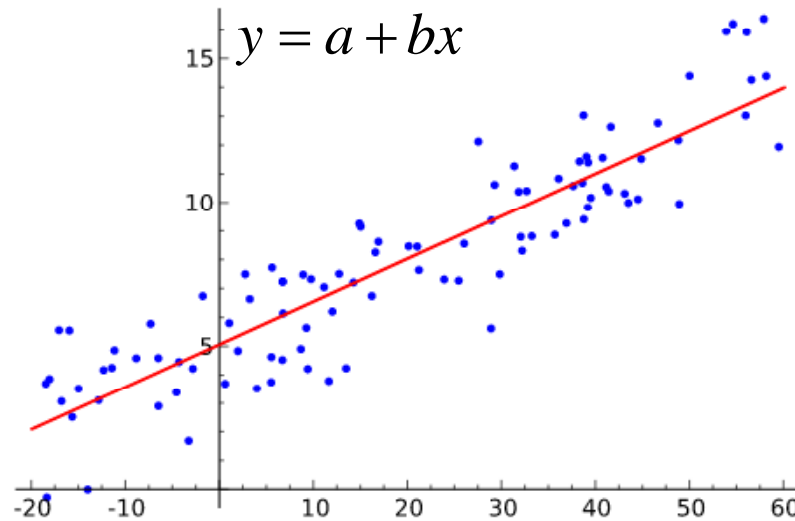
EXAMPLE: exponential. Normally this is done with the cumulative distribution

$$F_T(t) = 1 - e^{-\lambda t}$$



Do the points follow the simple exponential law? or maybe a Weibull $F_T(t) = 1 - e^{-(\lambda t)^\beta}$

Fitting data: least squares



Remember the goals:

- 1.- Parameter estimation
- 2.- Modelling (Hypothesis testing)

Goal: to minimize the “total distance” of n exp. points $d_1+d_2+\dots d_n$ to the model

or more seriously... to minimize the following variabel that follows a χ^2 -distribution and therefore **D is normally distributed** around H

$$\chi^2 = \sum_{i=1}^n \frac{(D_i - H_i)^2}{H_i}$$

Where D_i are the data pints, and H_i are the model expected values (Hypothesis)

... since for n large a χ^2 -distribution for point i tends to a gaussian with $\sigma^2=n=H_i$

$$\chi^2 = \sum_{i=1}^n \frac{(D_i - H_i)^2}{H_i} \rightarrow \sum_{i=1}^n \frac{(D_i - H_i)^2}{\sigma_i^2}$$

Fitting data: is the model right?

Let's do the question again (more precise):

- Is the χ^2 arising after minimization
- When assuming that the data are normally distributed around the model (hypothesis)
- Following a χ^2 -distribution of (as it should?)

Rule of thumb (or the joys of the χ^2 -distribution)



The χ^2 should follow a χ^2 -distribution with $n-m$ degrees of freedom arising for the data (with n points) and the model (with $m=2$ parameters)

For n data and 2 parameters $\mu=n-m$ and therefore the calculated χ^2 :

$$\chi^2 \approx (\mathbf{n-m})$$

For this reason it seems reasonable to define a reduced χ^2 that should be about one

$$\chi_{red}^2 = \frac{\chi^2}{n-m} \approx 1 \quad \dots \text{ for a good fit}$$

“Hypothesis testing”

Kolmogorov-Smirnov test: WE DO NOT NEED TO DECIDE A BINNING!!!!!!

1.- We calculate the cumulative distribution function CDF from the PDF and the model

$$CDF(\chi^2) = \int_0^{\chi^2} f(\chi^2) d\chi^2$$

2.- We look at the maximum distance between the model and the calculated CDF

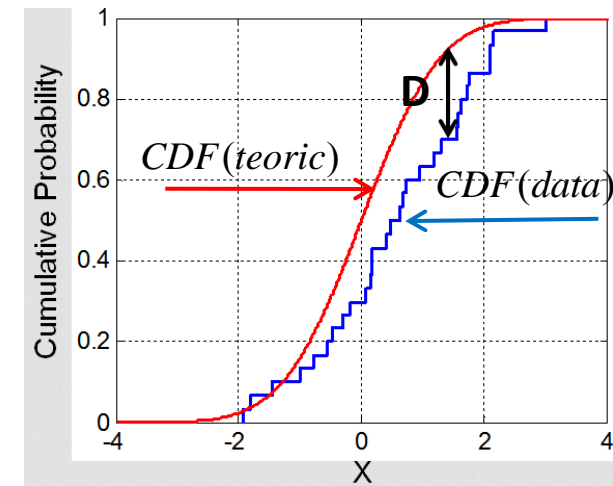
3.- We look at the table for confidence limits

confidence limit

Table 9.2: Critical Values of D_n^α in the Kolmogorov-Smirnov Test [9]

| $\alpha \backslash n$ | 0.20 | 0.10 | 0.05 | 0.01 |
|-----------------------|-------------------------|-------------------------|-------------------------|-------------------------|
| 5 | 0.45 | 0.51 | 0.56 | 0.67 |
| 10 | 0.32 | 0.37 | 0.41 | 0.49 |
| 15 | 0.27 | 0.30 | 0.34 | 0.40 |
| 20 | 0.23 | 0.26 | 0.29 | 0.36 |
| 25 | 0.21 | 0.24 | 0.27 | 0.32 |
| 30 | 0.19 | 0.22 | 0.24 | 0.29 |
| 35 | 0.18 | 0.20 | 0.23 | 0.27 |
| 40 | 0.17 | 0.19 | 0.21 | 0.25 |
| 45 | 0.16 | 0.18 | 0.20 | 0.24 |
| 50 | 0.15 | 0.17 | 0.19 | 0.23 |
| >50 | $\frac{1.07}{\sqrt{n}}$ | $\frac{1.22}{\sqrt{n}}$ | $\frac{1.36}{\sqrt{n}}$ | $\frac{1.63}{\sqrt{n}}$ |

number of data



Summary

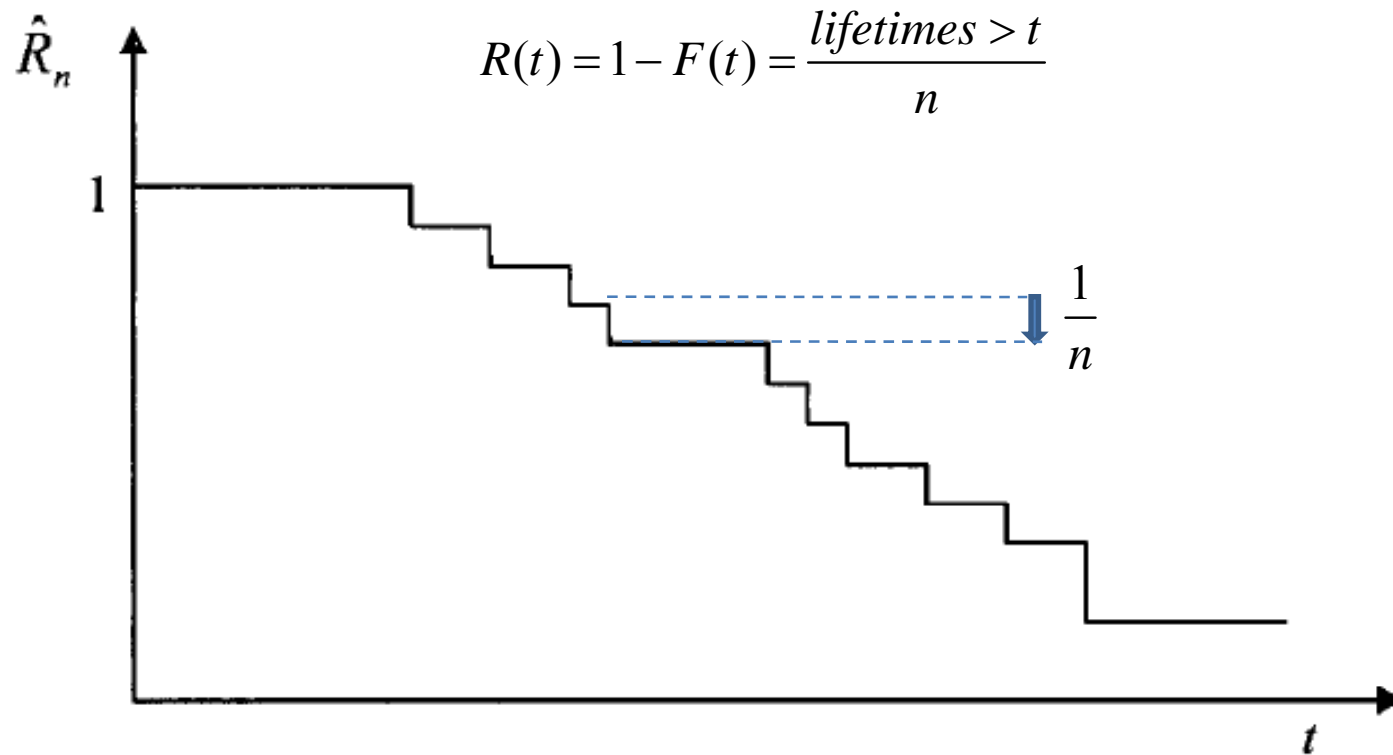
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ok... but i don't want to find a model. I want to directly the experimental CDF...

For a non-censored experiment this is quite easy!

Let's do it with the survival function $R(t)$:

t_i : is the lifetime of the unit $i=1,2,3,\dots n$



It must go down from 1 to 0 in n steps, therefore each step MUST be of height 1/n

KAPLAN-MEIER estimator

ok... but i don't want to find a model. I want to directly the experimental CDF...

For a censored experiment is not that easy!

Let's do it with the survival function $R(t)$:

t_i : is the lifetime of the unit $i=1,2,3,\dots n$

$(u_i, u_{i+1}]$: is an interval between u_i and u_{i+1} small enough that only a t_i falls into each interval

Let's calculate $R(t)$ at a time t_m

$$R(t_m) = P(T > t_m) = P(T > u_1 | T > u_0) \cdot P(T > u_2 | T > u_1) \cdot \dots \cdot P(T > t_m | T > u_m)$$

$$R(t_m) = P(T > t_m) = \prod_{i=0}^m P_i$$

$P_i = P(T > u_{i+1} | T > u_i)$

KAPLAN-MEIER estimator

The goal is to calculate P_i

$$R(t_m) = P(T > t_m) = \prod_{i=0}^m P_i$$
$$P_i = P(T > u_{i+1} | T > u_i)$$

remember:

Intervals $(u_j, u_{j+1}]$ are small enough so that maximum 1 failure occurs

1. If neither failure or censoring occurs $P_i=1$
2. If censoring occurs, no recording of failures occur, and again $P_i=1$
3. Imagine that a failure occurs in $(u_j, u_{j+1}]$.
The number of units at risk before are n_j
The number of units at risk after are n_j-1

$$P_i = P(T > u_{i+1} | T > u_i) = \frac{n_j - 1}{n_j}$$

Therefore the intervals where no failure occur can be disregarded

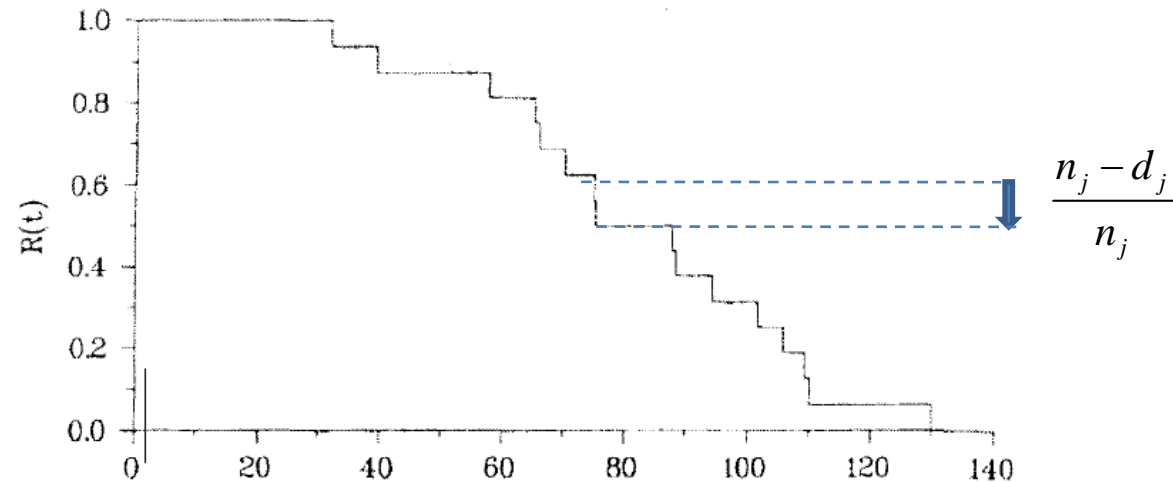
KAPLAN-MEIER estimator

Therefore, $R(t)$ will go down each time a component fail, and $R(t)$ can be represented as:

$$R(t_m) = P(T > t_m) = \prod_{i=0}^m P_i = \prod_{j=1}^{n_f} \frac{n_j - 1}{n_j}$$

If more than one unit fails at interval i , then if d_j units fail:

$$R(t_m) = P(T > t_m) = \prod_{i=0}^m P_i = \prod_{j=1}^{n_f} \frac{n_j - d_j}{n_j}$$



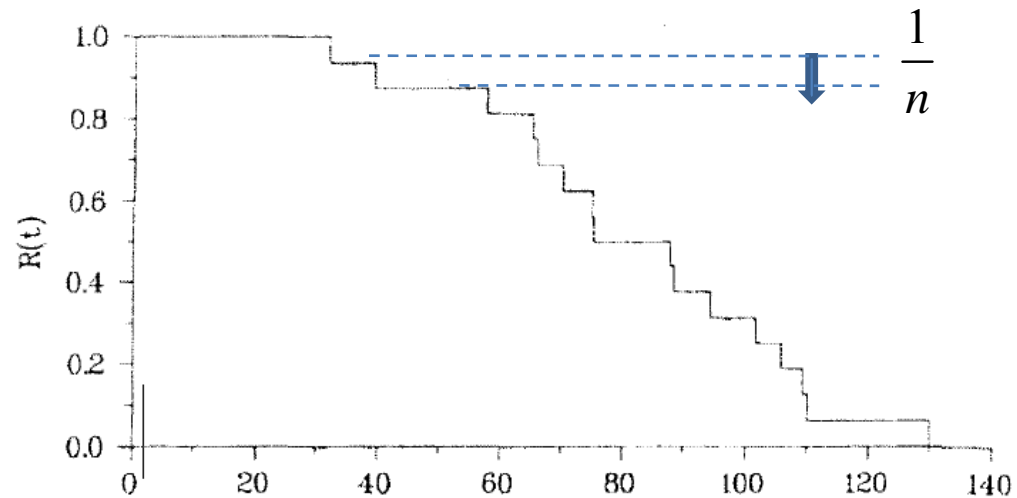
KAPLAN-MEIER estimator

EXAMPLE:

A test is carried out for $n=16$ units, obtaining the following failure times

31.7 ; 39.2 ; 57.5 ; 65.0 ; 65.8 ; 70.0 ; 75.0 ; 75.2 ;
87.5 ; 88.3 ; 94.2 ; 101.7 ; 105.8 ; 109.2 ; 110.0 ; 130.0

Calculate the survival function $R(t)$



KAPLAN-MEIER estimator

EXAMPLE (same times as before):

A test is carried out for $n=16$ units, obtaining the following failure times

31.7 ; 39.2 ; 57.5 ; 65.8 ; 70.0 ; 105.8 ; 110.0

The rest are censored tests Calculate the survival function $R(t)$

| Rank j | Inverse Rank $n-j+1$ | Ordered Failure and Censoring Times t_j | \hat{p}_j | $\hat{R}(t_{(j)})$ |
|----------|----------------------|-------------------------------------------|-------------|--------------------|
| 0 | - | - | 1 | 1.000 |
| 1 | 16 | 31.7 | 15/16 | 0.938 |
| 2 | 15 | 39.2 | 14/15 | 0.875 |
| 3 | 14 | 57.2 | 13/14 | 0.813 |
| 4 | 13 | 65.0* | 1 | 0.813 |
| 5 | 12 | 65.8 | 11/12 | 0.745 |
| 6 | 11 | 70.0 | 10/11 | 0.677 |
| 7 | 10 | 75.0* | 1 | 0.677 |
| 8 | 9 | 75.2* | 1 | 0.677 |
| 9 | 8 | 87.5* | 1 | 0.677 |
| 10 | 7 | 88.3* | 1 | 0.677 |
| 11 | 6 | 94.2* | 1 | 0.677 |
| 12 | 5 | 101.7* | 1 | 0.677 |
| 13 | 4 | 105.8 | 3/4 | 0.508 |
| 14 | 3 | 109.2* | 1 | 0.508 |
| 15 | 2 | 110.0 | 1/2 | 0.254 |
| 16 | 1 | 130.0* | 1 | 0.254 |



| t | $\hat{R}(t)$ |
|------------------------|---------------------------------------------|
| $0 \leq t < 31.7$ | =1 |
| $31.7 \leq t < 39.2$ | 15/16=0.938 |
| $39.2 \leq t < 57.5$ | 15/16·14/15=0.875 |
| $57.5 \leq t < 65.8$ | 15/16·14/15·13/14=0.813 |
| $65.8 \leq t < 70.0$ | 15/16·14/15·13/14·11/12=0.745 |
| $70.0 \leq t < 105.8$ | 15/16·14/15·13/14·11/12·10/11=0.677 |
| $105.8 \leq t < 110.0$ | 15/16·14/15·13/14·11/12·10/11·3/4=0.508 |
| $110.0 \leq t$ | 15/16·14/15·13/14·11/12·10/11·3/4·1/2=0.254 |

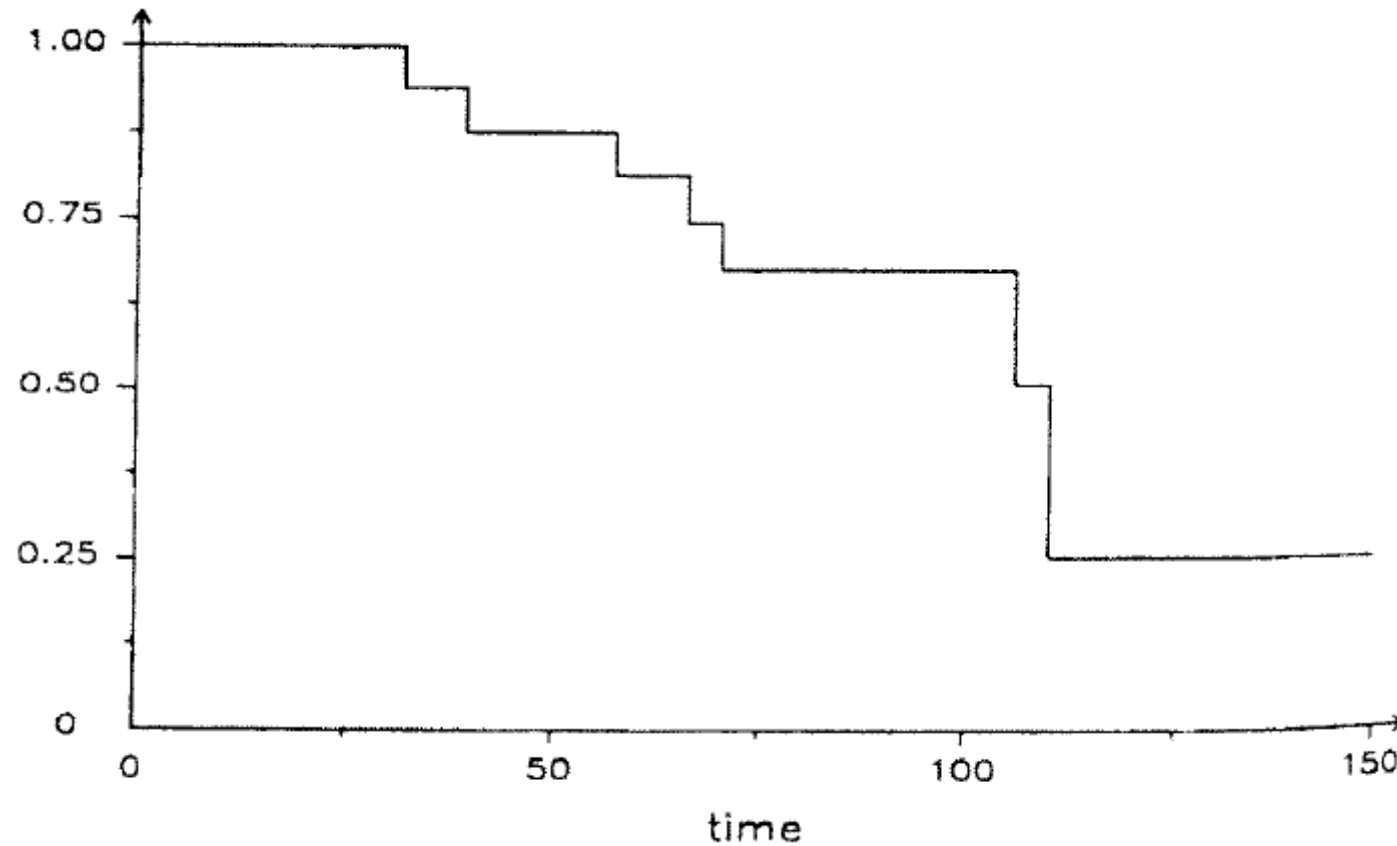
KAPLAN-MEIER estimator

EXAMPLE (same times as before):

A test is carried out for $n=16$ units, obtaining the following failure times

31.7 ; 39.2 ; 57.5 ; 65.8 ; 70.0 ; 105.8 ; 110.0

The rest are censored tests Calculate the survival function $R(t)$



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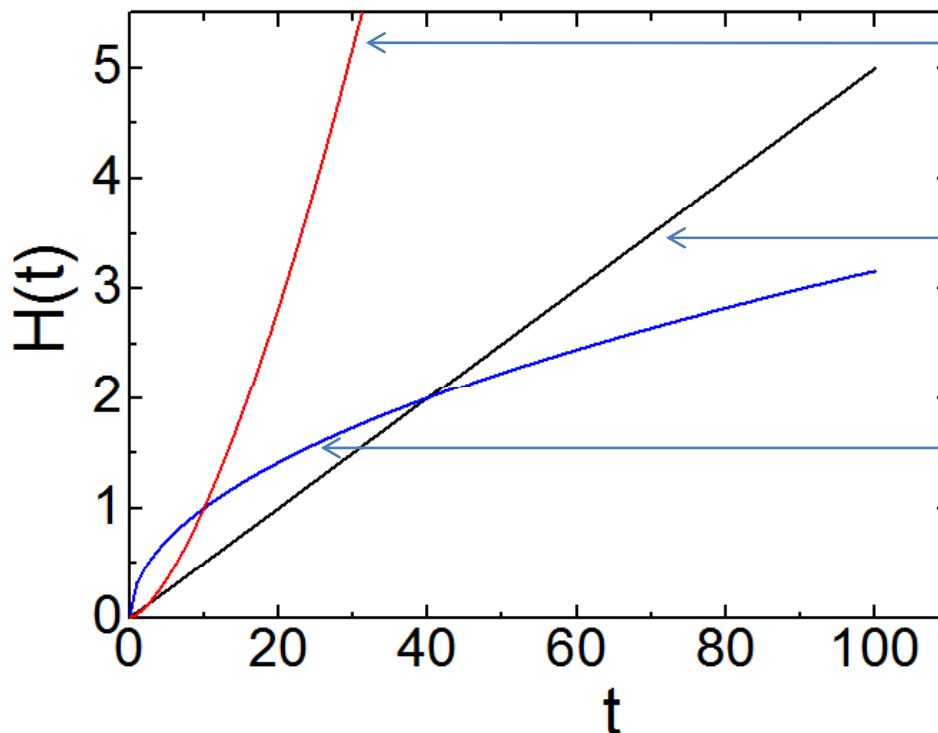
Reliability growth:

Engineering changes cause an increase of reliability

Can be quantified:

- Cumulative number of failures as a function of time
- Failure rate $h(t)=\lambda(t)$ as a function of time
- Mean time between failures (**MTBF**) as a function of time

We need, in any case, a reliability growth model



Duane model ($\beta > 0$)

$$H(t) = \left(\frac{t}{\tau}\right)^{\beta}$$



Exponential ($\beta = 0$)

$$H(t) = \lambda \cdot t = \frac{t}{\tau}$$

Duane model ($\beta < 0$)

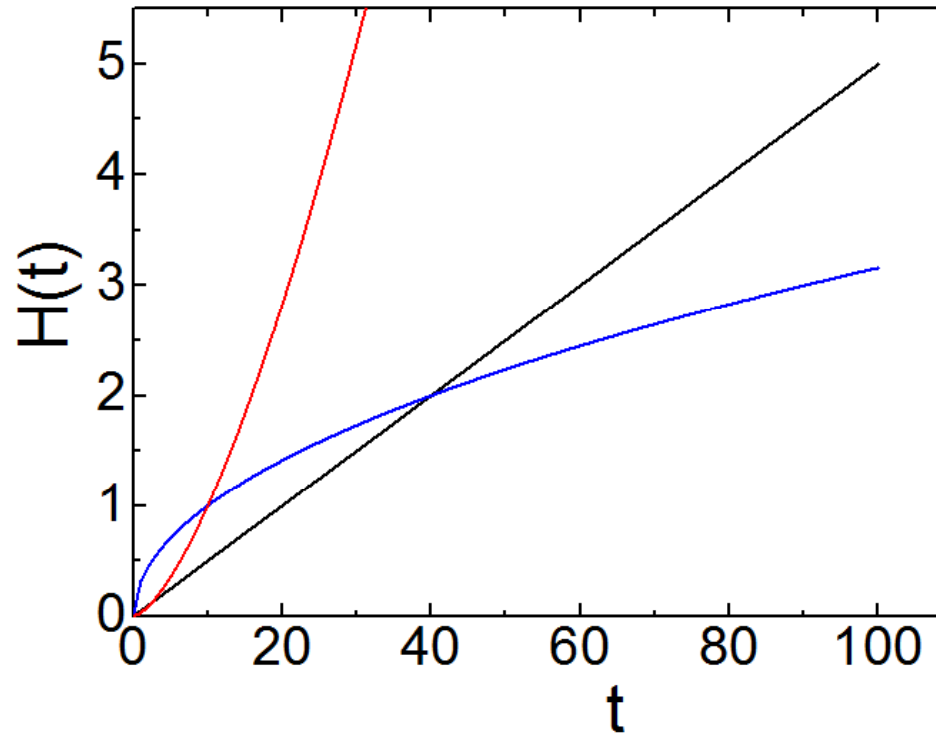
$$H(t) = \left(\frac{t}{\tau}\right)^{\beta}$$



Let's find the parameters of the Duane model: **Maximum likelihood**

Duane model ($\beta > 0$)

$$H(t) = \left(\frac{t}{\tau}\right)^\beta$$



Duane model ($\beta < 0$)

$$H(t) = \left(\frac{t}{\tau}\right)^\beta$$

Calculating de likelihood, making the logariothm and minimizing:

$$\hat{\beta} = \frac{n}{\sum_{i=1}^n \ln\left(\frac{T}{t_i}\right)} \quad \hat{\alpha} = \frac{T}{n^{1/\beta}}$$

Let's find the parameters of the Duane model: **Least squares**

Example:

Let's calculate the parameters of the Duane analysis for the following data

| (1) | (2) | (3) | (4) | (5) | (6) |
|--------------------|--------------------|----------------------|-----------------|--------------------------------------|---------------------------|
| Month of Operation | Hours of Operation | Cumulative Hours t | No. of failures | Cumulative Number of failures $H(t)$ | Cumulative MTBF $t/H'(t)$ |
| 1 | 541 | 541 | 3 | 3 | 180.3 |
| 2 | 1171 | 1712 | 5 | 8 | 214.0 |
| 3 | 1939 | 3651 | 4 | 12 | 304.3 |
| 4 | 2403 | 6054 | 1 | 13 | 465.7 |
| 5 | 1718 | 7772 | 2 | 15 | 518.1 |
| 6 | 2206 | 9978 | 2 | 17 | 586.9 |
| 7 | 1366 | 11244 | 3 | 20 | 562.2 |
| 8 | 1529 | 12873 | 0 | 20 | 643.7 |
| 9 | 1449 | 14322 | 2 | 22 | 651.0 |
| 10 | 1451 | 15773 | 2 | 24 | 657.2 |

Let's find the parameters of the Duane model: **Least squares**

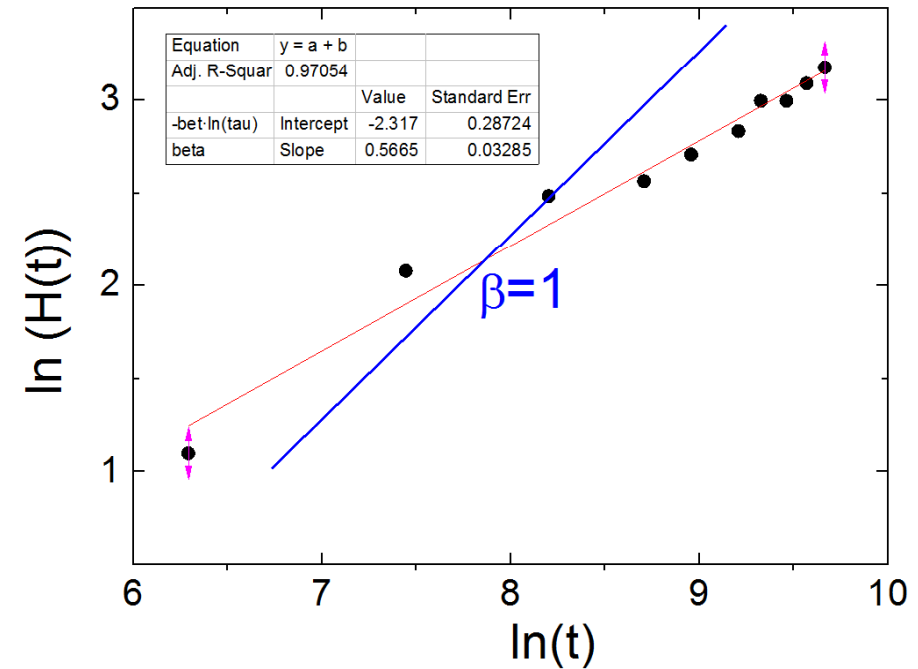
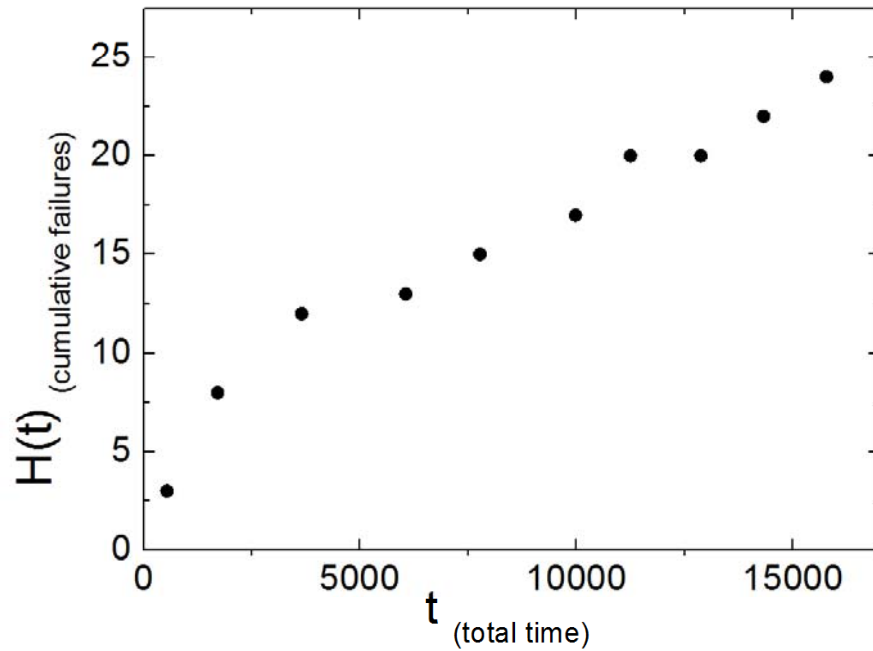
Let's first do the figure:

Duane Model

$$H(t) = \left(\frac{t}{\tau}\right)^\beta$$

linearized Duane Model

$$\ln(H(t)) = \beta \ln t - \beta \ln \tau$$



$\beta < 1$: reliability growth

Let's now add MONEY

Imagine a system whose failure causes production stoppage:

- Failure costs C_r (include production stoppage)
- Complete overhaul costs C_o (includes lost of production, replacement and labour)

What is the optimum overhaul policy?

The total cost is

$$C(t) = C_r H(t) + C_o \leftarrow \text{cost total overhaul}$$

↑ # units that fail
↑ cost to repair

And we just showed the Duane model for $H(t)$

$$H(t) = \left(\frac{t}{\tau} \right)^\beta$$

Therefore , the cost/unit operating time is

$$\gamma(t) = \frac{C(t)}{t} = \frac{C_r \left(\frac{t}{\tau} \right)^\beta + C_o}{t}$$

and we want o minimize this cost...

Therefore , the cost/unit operating time is

$$\gamma(t) = \frac{C(t)}{t} = \frac{C_r \left(\frac{t}{\tau} \right)^\beta + C_o}{t}$$

and we want o minimize this cost...

We solve the equation

$$\frac{d\gamma(t)}{dt} = 0$$

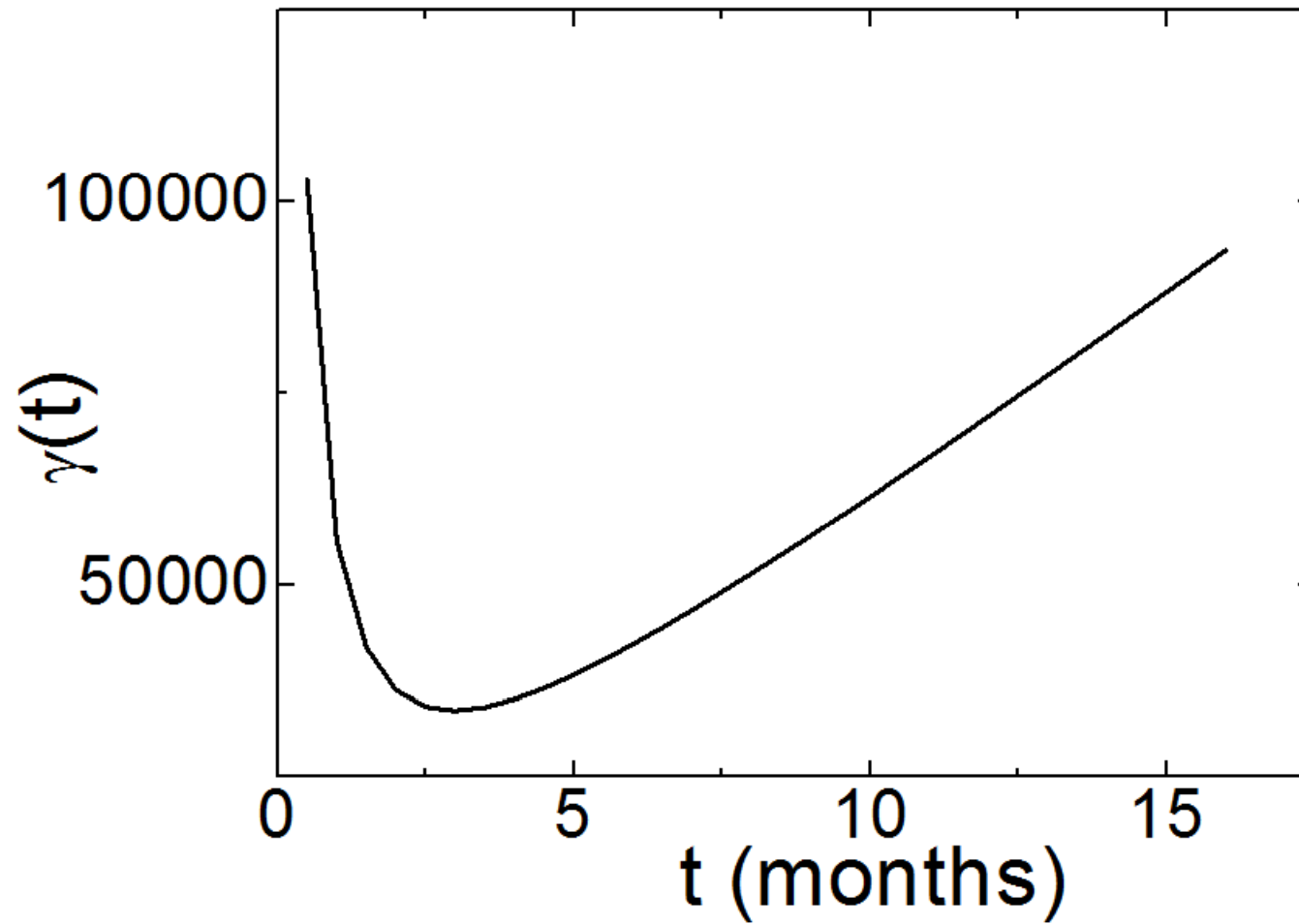
And we obtain that the optimal overhaul time is

$$t^* = \tau \left[\frac{\alpha^\beta C_o}{C_r (\beta - 1)} \right]^{1/\beta}$$

The overhaul time increases with C_o ... since it is expensive to do,
and increases with C_r , since if it is expensive is better to cahnge it

And the time is ∞ for $\beta=1$ (exponential)... therefore do never change

We can learn more looking at the cost/unit operating time

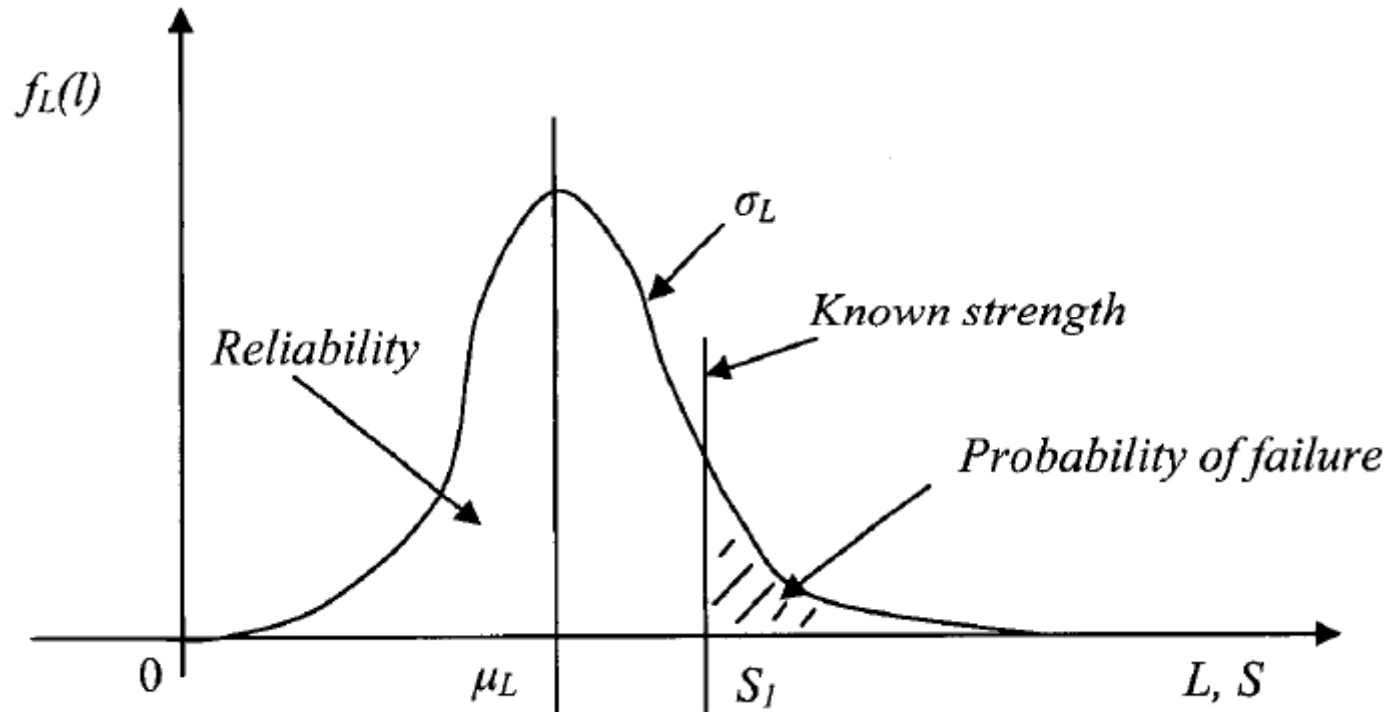


... when in doubt, do it later!

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Units fail when the **stress** is too high for their **strength**



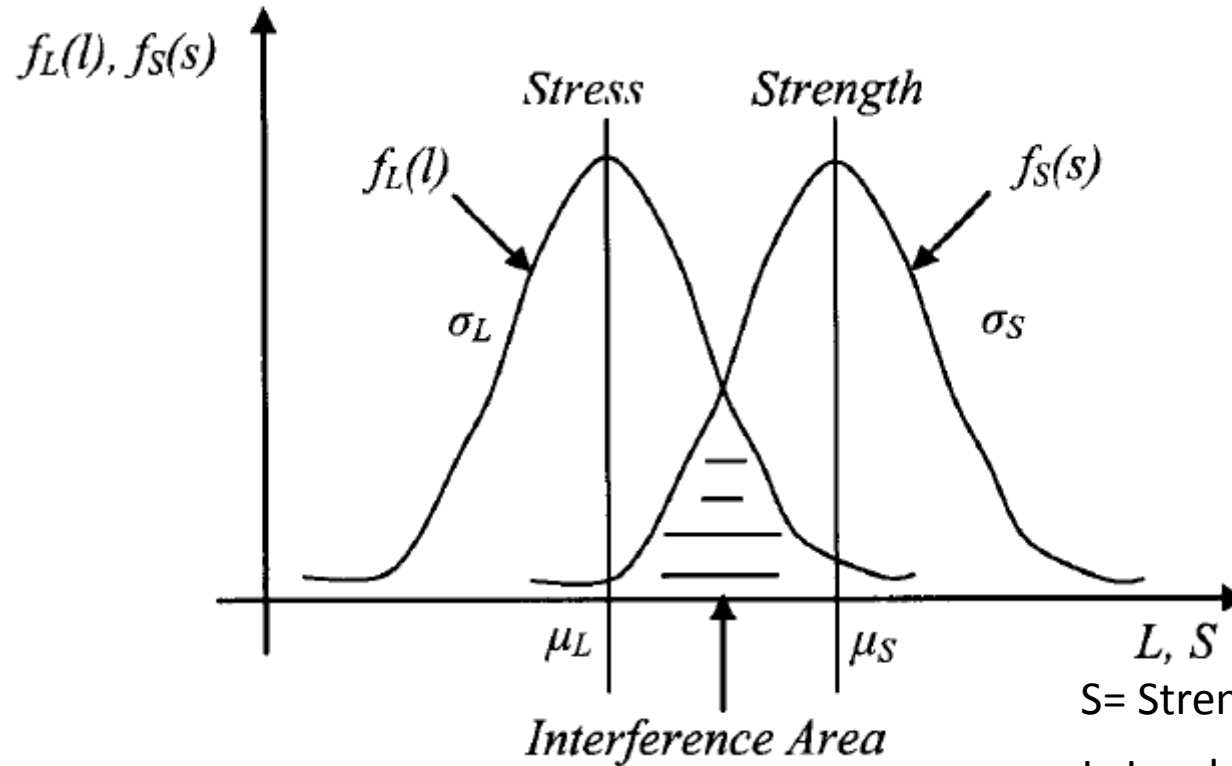
S= Strength of the unit

L=Load applied to the unit

Probability of failure:

$$F = P[L > S_1] = \int_{S_1}^{\infty} f(l) dl$$

Units fail when the **stress** is too high for their **strength** but stress might also have a probability distribution. Then

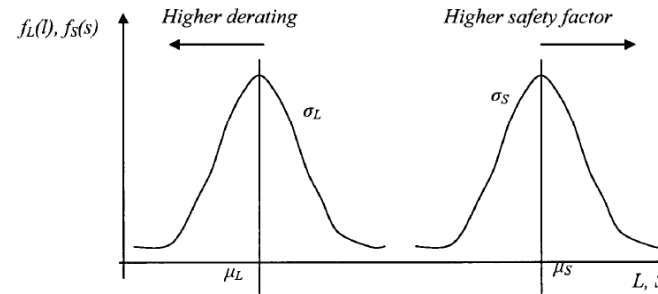


S= Strength of the unit

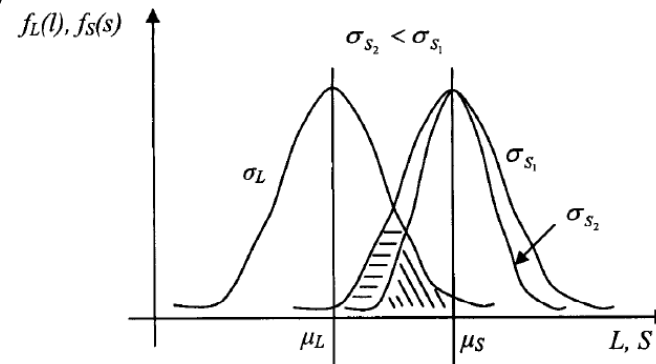
L=Load applied to the unit

To enhance the reliability there are three options

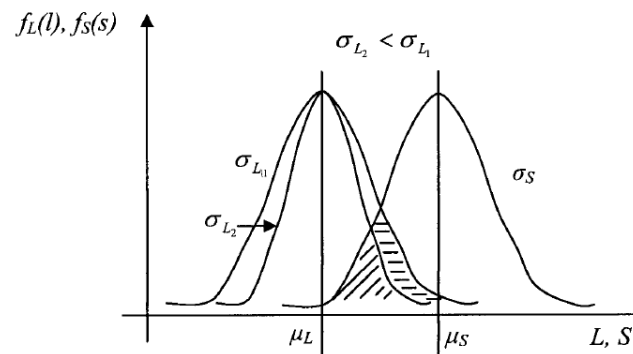
- Shift apart stress and strength distributions



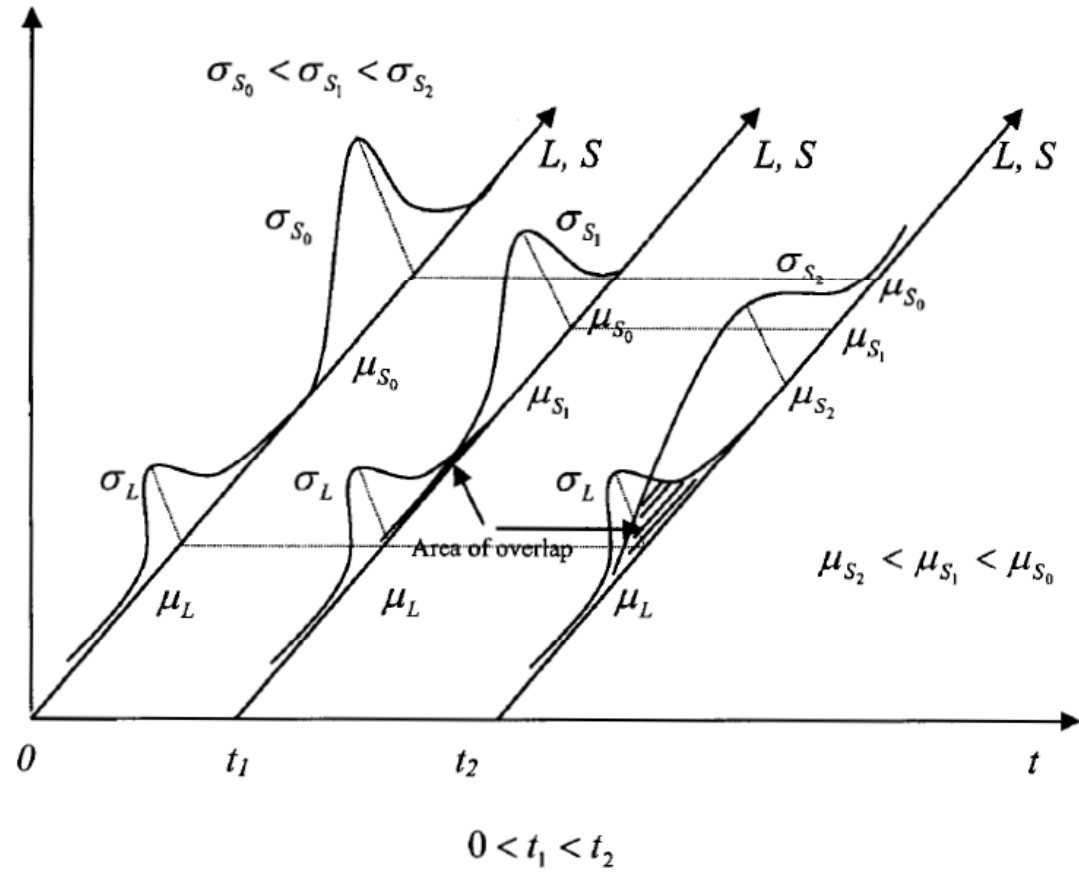
- Reduce the variability of stress



- Reduce the variability of strength (good quality controls!)



The problem is that strength varies over time while stress does not



A good quality

Appendix A: Table of Standard Normal Cumulative Distribution

$$F(\xi) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\xi} e^{-\frac{1}{2}x^2} dx$$

| ξ | $F(\xi)$ |
|-------|----------|
| 0.00 | 0.500000 |
| 0.01 | 0.503989 |
| 0.02 | 0.507978 |
| 0.03 | 0.511966 |
| 0.04 | 0.515954 |
| 0.05 | 0.519939 |
| 0.06 | 0.523922 |
| 0.07 | 0.527904 |
| 0.08 | 0.531882 |
| 0.09 | 0.535857 |
| 0.10 | 0.539828 |
| 0.11 | 0.543796 |
| 0.12 | 0.547759 |
| 0.13 | 0.551717 |
| 0.14 | 0.555671 |
| 0.15 | 0.559618 |
| 0.16 | 0.563500 |
| 0.17 | 0.567494 |
| 0.18 | 0.571423 |
| 0.19 | 0.575345 |
| 0.20 | 0.579260 |
| 0.21 | 0.583166 |
| 0.22 | 0.587064 |
| 0.23 | 0.590954 |
| 0.24 | 0.549835 |
| 0.25 | 0.598706 |
| 0.26 | 0.602568 |
| 0.27 | 0.606420 |
| 0.28 | 0.610262 |
| 0.29 | 0.614092 |

| ξ | $F(\xi)$ |
|-------|----------|
| 0.50 | 0.691463 |
| 0.51 | 0.694975 |
| 0.52 | 0.698468 |
| 0.53 | 0.701944 |
| 0.54 | 0.705401 |
| 0.55 | 0.708840 |
| 0.56 | 0.712260 |
| 0.57 | 0.715661 |
| 0.58 | 0.719043 |
| 0.59 | 0.722405 |
| 0.60 | 0.725747 |
| 0.61 | 0.729069 |
| 0.62 | 0.732371 |
| 0.63 | 0.735653 |
| 0.64 | 0.738914 |
| 0.65 | 0.742154 |
| 0.66 | 0.745374 |
| 0.67 | 0.748572 |
| 0.68 | 0.751748 |
| 0.69 | 0.754903 |
| 0.70 | 0.758036 |
| 0.71 | 0.761148 |
| 0.72 | 0.764238 |
| 0.73 | 0.767305 |
| 0.74 | 0.770350 |
| 0.75 | 0.773373 |
| 0.76 | 0.776373 |
| 0.77 | 0.779350 |
| 0.78 | 0.782305 |
| 0.79 | 0.785236 |

| ξ | $F(\xi)$ |
|-------|----------|
| 1.00 | 0.841345 |
| 1.01 | 0.843752 |
| 1.02 | 0.846136 |
| 1.03 | 0.848495 |
| 1.04 | 0.850830 |
| 1.05 | 0.853141 |
| 1.06 | 0.855428 |
| 1.07 | 0.857690 |
| 1.08 | 0.859929 |
| 1.09 | 0.862143 |
| 1.10 | 0.864334 |
| 1.11 | 0.866500 |
| 1.12 | 0.868643 |
| 1.13 | 0.870762 |
| 1.14 | 0.872857 |
| 1.15 | 0.874928 |
| 1.16 | 0.876976 |
| 1.17 | 0.878999 |
| 1.18 | 0.881000 |
| 1.19 | 0.882977 |
| 1.20 | 0.884930 |
| 1.21 | 0.886860 |
| 1.22 | 0.888767 |
| 1.23 | 0.890651 |
| 1.24 | 0.892512 |
| 1.25 | 0.894350 |
| 1.26 | 0.896165 |
| 1.27 | 0.897958 |
| 1.28 | 0.899727 |
| 1.29 | 0.901475 |

| ξ | $F(\xi)$ |
|-------|----------|
| 0.30 | 0.617912 |
| 0.31 | 0.621720 |
| 0.32 | 0.623517 |
| 0.33 | 0.629301 |
| 0.34 | 0.633072 |
| 0.35 | 0.636831 |
| 0.36 | 0.640576 |
| 0.37 | 0.644309 |
| 0.38 | 0.648027 |
| 0.39 | 0.651732 |
| 0.40 | 0.655422 |
| 0.41 | 0.659097 |
| 0.42 | 0.662757 |
| 0.43 | 0.666402 |
| 0.44 | 0.670032 |
| 0.45 | 0.673645 |
| 0.46 | 0.677242 |
| 0.47 | 0.680823 |
| 0.48 | 0.684387 |
| 0.49 | 0.687933 |
| 1.50 | 0.933193 |
| 1.51 | 0.934478 |
| 1.52 | 0.935744 |
| 1.53 | 0.936992 |
| 1.54 | 0.938220 |
| 1.55 | 0.939429 |
| 1.56 | 0.940620 |
| 1.57 | 0.941792 |
| 1.58 | 0.942947 |
| 1.59 | 0.944083 |
| 1.60 | 0.945201 |
| 1.61 | 0.946301 |
| 1.62 | 0.947384 |
| 1.63 | 0.948449 |
| 1.64 | 0.949497 |

| ξ | $F(\xi)$ |
|-------|----------|
| 0.80 | 0.788145 |
| 0.81 | 0.791030 |
| 0.82 | 0.793892 |
| 0.83 | 0.796731 |
| 0.84 | 0.799546 |
| 0.85 | 0.802337 |
| 0.86 | 0.805105 |
| 0.87 | 0.807850 |
| 0.88 | 0.810570 |
| 0.89 | 0.813267 |
| 0.90 | 0.815940 |
| 0.91 | 0.818589 |
| 0.92 | 0.821214 |
| 0.93 | 0.823815 |
| 0.94 | 0.826391 |
| 0.95 | 0.828944 |
| 0.96 | 0.831473 |
| 0.97 | 0.833977 |
| 0.98 | 0.836457 |
| 0.99 | 0.838913 |
| 2.00 | 0.977250 |
| 2.01 | 0.977784 |
| 2.02 | 0.978308 |
| 2.03 | 0.978822 |
| 2.04 | 0.979325 |
| 2.05 | 0.979818 |
| 2.06 | 0.980301 |
| 2.07 | 0.980774 |
| 2.08 | 0.981237 |
| 2.09 | 0.981691 |
| 2.10 | 0.982136 |
| 2.11 | 0.982571 |
| 2.12 | 0.982997 |
| 2.13 | 0.983414 |
| 2.14 | 0.983823 |

| ξ | $F(\xi)$ |
|-------|----------|
| 1.30 | 0.903199 |
| 1.31 | 0.904902 |
| 1.32 | 0.906583 |
| 1.33 | 0.908241 |
| 1.34 | 0.909877 |
| 1.35 | 0.911492 |
| 1.36 | 0.913085 |
| 1.37 | 0.914656 |
| 1.38 | 0.916207 |
| 1.39 | 0.917735 |
| 1.40 | 0.919243 |
| 1.41 | 0.920730 |
| 1.42 | 0.922196 |
| 1.43 | 0.923641 |
| 1.44 | 0.925066 |
| 1.45 | 0.926471 |
| 1.46 | 0.927855 |
| 1.47 | 0.929219 |
| 1.48 | 0.930563 |
| 1.49 | 0.931888 |
| 2.50 | 0.993790 |
| 2.51 | 0.993963 |
| 2.52 | 0.994132 |
| 2.53 | 0.994267 |
| 2.54 | 0.994457 |
| 2.55 | 0.994614 |
| 2.56 | 0.994766 |
| 2.57 | 0.994915 |
| 2.58 | 0.995060 |
| 2.59 | 0.995201 |
| 2.60 | 0.995339 |
| 2.61 | 0.995473 |
| 2.62 | 0.995604 |
| 2.63 | 0.995731 |
| 2.64 | 0.995855 |

| ξ | $F(\xi)$ |
|-------|----------|
| 1.65 | 0.950529 |
| 1.66 | 0.951543 |
| 1.67 | 0.952540 |
| 1.68 | 0.953521 |
| 1.69 | 0.954486 |
| | |
| 1.70 | 0.955435 |
| 1.71 | 0.956367 |
| 1.72 | 0.957284 |
| 1.73 | 0.958185 |
| 1.74 | 0.959071 |
| | |
| 1.75 | 0.959941 |
| 1.76 | 0.960796 |
| 1.77 | 0.961636 |
| 1.78 | 0.962426 |
| 1.79 | 0.963273 |
| | |
| 1.80 | 0.964070 |
| 1.81 | 0.964852 |
| 1.82 | 0.965621 |
| 1.83 | 0.966375 |
| 1.84 | 0.967116 |
| | |
| 1.85 | 0.967843 |
| 1.86 | 0.968557 |
| 1.87 | 0.969258 |
| 1.88 | 0.969946 |
| 1.89 | 0.970621 |
| | |
| 1.90 | 0.971284 |
| 1.91 | 0.971933 |
| 1.92 | 0.972571 |
| 1.93 | 0.973197 |
| 1.94 | 0.973810 |
| | |
| 1.95 | 0.974412 |
| 1.96 | 0.975002 |
| 1.97 | 0.975581 |
| 1.98 | 0.976148 |
| 1.99 | 0.976705 |

| ξ | $F(\xi)$ |
|-------|----------|
| 2.15 | 0.984223 |
| 2.16 | 0.984614 |
| 2.17 | 0.984997 |
| 2.18 | 0.985371 |
| 2.19 | 0.985738 |
| | |
| 2.20 | 0.986097 |
| 2.21 | 0.986447 |
| 2.22 | 0.986791 |
| 2.23 | 0.987126 |
| 2.24 | 0.987455 |
| | |
| 2.25 | 0.987776 |
| 2.26 | 0.988089 |
| 2.27 | 0.988396 |
| 2.28 | 0.988696 |
| 2.29 | 0.988989 |
| | |
| 2.30 | 0.989276 |
| 2.31 | 0.989556 |
| 2.32 | 0.989830 |
| 2.33 | 0.990097 |
| 2.34 | 0.990358 |
| | |
| 2.35 | 0.990613 |
| 2.36 | 0.990863 |
| 2.37 | 0.991106 |
| 2.38 | 0.991344 |
| 2.39 | 0.991576 |
| | |
| 2.40 | 0.991802 |
| 2.41 | 0.992024 |
| 2.42 | 0.992240 |
| 2.43 | 0.992451 |
| 2.44 | 0.992656 |
| | |
| 2.45 | 0.992857 |
| 2.46 | 0.993053 |
| 2.47 | 0.993244 |
| 2.48 | 0.993431 |
| 2.49 | 0.993613 |

| ξ | $F(\xi)$ |
|-------|----------|
| 2.65 | 0.995975 |
| 2.66 | 0.996093 |
| 2.67 | 0.996207 |
| 2.68 | 0.996319 |
| 2.69 | 0.996427 |
| | |
| 2.70 | 0.996533 |
| 2.71 | 0.996636 |
| 2.72 | 0.996736 |
| 2.73 | 0.996833 |
| 2.74 | 0.996928 |
| | |
| 2.75 | 0.997020 |
| 2.76 | 0.997110 |
| 2.77 | 0.997197 |
| 2.78 | 0.997282 |
| 2.79 | 0.997365 |
| | |
| 2.80 | 0.997445 |
| 2.81 | 0.997523 |
| 2.82 | 0.997599 |
| 2.83 | 0.997673 |
| 2.84 | 0.997744 |
| | |
| 2.85 | 0.997814 |
| 2.86 | 0.997882 |
| 2.87 | 0.997948 |
| 2.88 | 0.998012 |
| 2.89 | 0.998074 |
| | |
| 2.90 | 0.998134 |
| 2.91 | 0.998193 |
| 2.92 | 0.998250 |
| 2.93 | 0.998305 |
| 2.94 | 0.998359 |
| | |
| 2.95 | 0.998411 |
| 2.96 | 0.998462 |
| 2.97 | 0.998511 |
| 2.98 | 0.998559 |
| 2.99 | 0.998605 |

| ξ | $F(\xi)$ |
|-------|----------|
| 3.00 | 0.998630 |
| 3.01 | 0.998694 |
| 3.02 | 0.998736 |
| 3.03 | 0.998777 |
| 3.04 | 0.998817 |
| | |
| 3.05 | 0.998856 |
| 3.06 | 0.998893 |
| 3.07 | 0.998930 |
| 3.08 | 0.998965 |
| 3.09 | 0.998999 |
| | |
| 3.10 | 0.999032 |
| 3.11 | 0.999065 |
| 3.12 | 0.999096 |
| 3.13 | 0.999126 |
| 3.14 | 0.999155 |
| | |
| 3.15 | 0.992184 |
| 3.16 | 0.999119 |
| 3.17 | 0.999238 |
| 3.18 | 0.999264 |
| 3.19 | 0.999289 |
| | |
| 3.20 | 0.999313 |
| 3.21 | 0.999336 |
| 3.22 | 0.999359 |
| 3.23 | 0.999381 |
| 3.24 | 0.999402 |
| | |
| 3.25 | 0.999423 |
| 3.26 | 0.999443 |
| 3.27 | 0.999462 |
| 3.28 | 0.999481 |
| 3.29 | 0.999499 |
| | |
| 3.30 | 0.999516 |
| 3.31 | 0.999533 |
| 3.32 | 0.999550 |
| 3.33 | 0.999566 |
| 3.34 | 0.999581 |

| ξ | $F(\xi)$ |
|-------|----------|
| 3.50 | 0.999767 |
| 3.51 | 0.999776 |
| 3.52 | 0.999784 |
| 3.53 | 0.999792 |
| 3.54 | 0.999800 |
| | |
| 3.55 | 0.999807 |
| 3.56 | 0.999815 |
| 3.57 | 0.999821 |
| 3.58 | 0.999828 |
| 3.59 | 0.999835 |
| | |
| 3.60 | 0.999841 |
| 3.61 | 0.999847 |
| 3.62 | 0.999853 |
| 3.63 | 0.999858 |
| 3.64 | 0.999864 |
| | |
| 3.65 | 0.999869 |
| 3.66 | 0.999874 |
| 3.67 | 0.999879 |
| 3.68 | 0.999883 |
| 3.69 | 0.999888 |
| | |
| 3.70 | 0.999892 |
| 3.71 | 0.999896 |
| 3.72 | 0.999900 |
| 3.73 | 0.999904 |
| 3.74 | 0.999908 |
| | |
| 3.75 | 0.999912 |
| 3.76 | 0.999915 |
| 3.77 | 0.999918 |
| 3.78 | 0.999922 |
| 3.79 | 0.999925 |
| | |
| 3.80 | 0.999928 |
| 3.81 | 0.999931 |
| 3.82 | 0.999933 |
| 3.83 | 0.999936 |
| 3.84 | 0.999938 |

| ξ | $1-F(\xi)$ |
|-------|--------------|
| 4.00 | 0.316712E-04 |
| 4.05 | 0.256088E-04 |
| 4.10 | 0.206575E-04 |
| 4.15 | 0.166238E-04 |
| 4.20 | 0.133458E-04 |
| | |
| 4.25 | 0.106883E-04 |
| 4.30 | 0.853906E-05 |
| 4.35 | 0.680688E-05 |
| 4.40 | 0.541234E-05 |
| 4.45 | 0.429351E-05 |
| | |
| 4.50 | 0.339767E-05 |
| 4.55 | 0.268230E-05 |
| 4.60 | 0.211245E-05 |
| 4.65 | 0.165968E-05 |
| 4.70 | 0.130081E-05 |
| | |
| 4.75 | 0.101708E-05 |
| 4.80 | 0.793328E-06 |
| 4.85 | 0.617307E-06 |
| 4.90 | 0.479183E-06 |
| 4.95 | 0.371067E-06 |
| | |
| 5.00 | 0.286652E-06 |
| 5.10 | 0.169827E-06 |
| 5.20 | 0.996443E-07 |
| 5.30 | 0.579013E-07 |
| 5.40 | 0.333204E-07 |
| | |
| 5.50 | 0.189896E-07 |
| 5.60 | 0.107176E-07 |
| 5.70 | 0.599037E-08 |
| 5.80 | 0.331575E-08 |
| 5.90 | 0.181751E-08 |
| | |
| 6.00 | 0.986588E-09 |
| 6.10 | 0.530343E-09 |
| 6.20 | 0.282316E-09 |
| 6.30 | 0.148823E-09 |
| 6.40 | 0.77688 E-10 |

| ξ | $F(\xi)$ |
|-------|----------|
| 3.35 | 0.999596 |
| 3.36 | 0.999610 |
| 3.37 | 0.999624 |
| 3.38 | 0.999637 |
| 3.39 | 0.999650 |
| | |
| 3.40 | 0.999663 |
| 3.41 | 0.999675 |
| 3.42 | 0.999687 |
| 3.43 | 0.999698 |
| 3.44 | 0.999709 |
| | |
| 3.45 | 0.999720 |
| 3.46 | 0.999730 |
| 3.47 | 0.999740 |
| 3.48 | 0.999749 |
| 3.49 | 0.999758 |

| ξ | $F(\xi)$ |
|-------|----------|
| 3.85 | 0.999941 |
| 3.86 | 0.999943 |
| 3.87 | 0.999946 |
| 3.88 | 0.999948 |
| 3.89 | 0.999950 |
| | |
| 3.90 | 0.999952 |
| 3.91 | 0.999954 |
| 3.92 | 0.999956 |
| 3.93 | 0.999958 |
| 3.94 | 0.999959 |
| | |
| 3.95 | 0.999961 |
| 3.96 | 0.999963 |
| 3.97 | 0.999964 |
| 3.98 | 0.999966 |
| 3.99 | 0.999967 |


| ξ | $1-F(\xi)$ |
|-------|--------------|
| 6.50 | 0.40160 E-10 |
| 6.60 | 0.20558 E-10 |
| 6.70 | 0.10421 E-10 |
| 6.80 | 0.5231 E-11 |
| 6.90 | 0.260 E-11 |
| | |
| 7.00 | 0.128 E-11 |
| 7.10 | 0.624 E-12 |
| 7.20 | 0.301 E-12 |
| 7.30 | 0.144 E-12 |
| 7.40 | 0.68 E-13 |
| | |
| 7.50 | 0.32 E-13 |
| 7.60 | 0.15 E-13 |
| 7.70 | 0.70 E-14 |
| 7.80 | 0.30 E-14 |
| 7.90 | 0.15 E-14 |

Appendix B: Table of Chi-Square Cumulative Distribution

$\chi^2_\alpha(f)$

| $f \setminus \alpha$ | 0.995 | 0.99 | 0.975 | 0.95 | 0.90 | 0.10 | 0.05 | 0.025 | 0.01 | 0.005 |
|----------------------|--------|--------|--------|--------|--------|---------|---------|---------|---------|---------|
| 1 | — | — | 0.001 | 0.004 | 0.016 | 2.706 | 3.841 | 5.024 | 6.635 | 7.879 |
| 2 | 0.010 | 0.020 | 0.051 | 0.103 | 0.211 | 4.605 | 5.991 | 7.378 | 9.210 | 10.597 |
| 3 | 0.072 | 0.115 | 0.216 | 0.352 | 0.584 | 6.251 | 7.815 | 9.348 | 11.345 | 12.838 |
| 4 | 0.207 | 0.297 | 0.484 | 0.711 | 1.064 | 7.779 | 9.488 | 11.143 | 13.277 | 14.860 |
| 5 | 0.412 | 0.554 | 0.831 | 1.145 | 1.610 | 9.236 | 11.070 | 12.833 | 15.086 | 16.750 |
| 6 | 0.676 | 0.872 | 1.237 | 1.635 | 2.204 | 10.645 | 12.592 | 14.449 | 16.812 | 18.548 |
| 7 | 0.989 | 1.239 | 1.690 | 2.167 | 2.833 | 12.017 | 14.067 | 16.013 | 18.475 | 20.278 |
| 8 | 1.344 | 1.646 | 2.180 | 2.733 | 3.490 | 13.362 | 15.507 | 17.535 | 20.090 | 21.955 |
| 9 | 1.735 | 2.088 | 2.700 | 3.325 | 4.168 | 14.684 | 16.919 | 19.023 | 21.666 | 23.589 |
| 10 | 2.156 | 2.558 | 3.247 | 3.940 | 4.865 | 15.987 | 18.307 | 20.483 | 23.209 | 25.188 |
| 11 | 2.603 | 3.053 | 3.816 | 4.575 | 5.578 | 17.275 | 19.675 | 21.920 | 24.725 | 26.757 |
| 12 | 3.074 | 3.571 | 4.404 | 5.226 | 6.304 | 18.549 | 21.026 | 23.337 | 26.217 | 28.300 |
| 13 | 3.565 | 4.107 | 5.009 | 5.892 | 7.042 | 19.812 | 22.362 | 24.736 | 27.688 | 29.819 |
| 14 | 4.075 | 4.660 | 5.629 | 6.571 | 7.790 | 21.064 | 23.685 | 26.119 | 29.141 | 31.319 |
| 15 | 4.601 | 5.229 | 6.262 | 7.261 | 8.547 | 22.307 | 24.996 | 27.488 | 30.578 | 32.801 |
| 16 | 5.142 | 5.812 | 6.908 | 7.962 | 9.312 | 23.542 | 26.296 | 28.845 | 32.000 | 34.267 |
| 17 | 5.697 | 6.408 | 7.564 | 8.672 | 10.085 | 24.769 | 27.587 | 30.191 | 33.409 | 35.718 |
| 18 | 6.265 | 7.015 | 8.231 | 9.390 | 10.865 | 25.989 | 28.869 | 31.526 | 34.805 | 37.156 |
| 19 | 6.844 | 7.633 | 8.907 | 10.117 | 11.651 | 27.204 | 30.144 | 32.852 | 36.191 | 38.582 |
| 20 | 7.434 | 8.260 | 9.591 | 10.851 | 12.443 | 28.412 | 31.410 | 34.170 | 37.566 | 39.997 |
| 21 | 8.034 | 8.897 | 10.283 | 11.591 | 13.240 | 29.615 | 32.671 | 35.479 | 38.932 | 41.401 |
| 22 | 8.643 | 9.542 | 10.982 | 12.338 | 14.041 | 30.813 | 33.924 | 36.781 | 40.289 | 42.796 |
| 23 | 9.260 | 10.196 | 11.689 | 13.091 | 14.848 | 32.007 | 35.172 | 38.076 | 41.638 | 44.181 |
| 24 | 9.886 | 10.856 | 12.401 | 13.848 | 15.659 | 33.196 | 36.415 | 39.364 | 42.980 | 45.559 |
| 25 | 10.520 | 11.524 | 13.120 | 14.611 | 16.473 | 34.382 | 37.652 | 40.646 | 44.314 | 46.928 |
| 26 | 11.160 | 12.198 | 13.844 | 15.379 | 17.292 | 35.563 | 38.885 | 41.923 | 45.642 | 48.290 |
| 27 | 11.808 | 12.879 | 14.573 | 16.151 | 18.114 | 36.741 | 40.113 | 43.195 | 46.963 | 49.645 |
| 28 | 12.461 | 13.565 | 15.308 | 16.928 | 18.939 | 37.916 | 41.337 | 44.461 | 48.278 | 50.993 |
| 29 | 13.121 | 14.256 | 16.047 | 17.708 | 19.768 | 39.087 | 42.557 | 45.722 | 49.588 | 52.336 |
| 30 | 13.787 | 14.953 | 16.791 | 18.493 | 20.599 | 40.256 | 43.773 | 46.979 | 50.892 | 53.672 |
| 40 | 20.707 | 22.164 | 24.433 | 26.509 | 29.051 | 51.805 | 55.758 | 59.342 | 63.691 | 66.766 |
| 50 | 27.991 | 29.707 | 32.357 | 34.764 | 37.689 | 63.167 | 67.505 | 71.420 | 76.154 | 79.490 |
| 60 | 35.534 | 37.485 | 40.482 | 43.188 | 46.459 | 74.397 | 79.082 | 83.298 | 88.379 | 91.952 |
| 70 | 43.275 | 45.442 | 48.758 | 51.739 | 55.329 | 85.527 | 90.531 | 95.023 | 100.425 | 104.215 |
| 80 | 51.172 | 53.540 | 57.153 | 60.391 | 64.278 | 96.578 | 101.879 | 106.629 | 112.329 | 116.321 |
| 90 | 59.196 | 61.754 | 65.647 | 69.126 | 73.291 | 107.565 | 113.145 | 118.136 | 124.116 | 128.299 |
| 100 | 67.328 | 70.065 | 74.222 | 77.929 | 82.358 | 118.498 | 124.342 | 129.561 | 135.807 | 140.169 |

$$f(x) = A \cdot x^{k/2-1} e^{-x/2}$$



$$A = \frac{1}{2^{k/2} \Gamma(k/2)}$$